

1 **A review on membrane fouling control in anaerobic membrane bioreactors**  
2 **by adding performance enhancers**

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15  
16 **Abstract**

17 Anaerobic membrane bioreactors (AnMBRs), the combination of anaerobic digestion and  
18 membrane technology, have gained increasing popularity due to their remarkable advantages  
19 over aerobic membrane bioreactors, such as biogas production and potential energy use.  
20 However, membrane fouling remains a challenging issue that deteriorates the performance of  
21 membrane and shortens its lifespan. Pretreatment of feed wastewater by adding fouling  
22 reduction enhancers, such as adsorbents and flocculants, into anaerobic membrane bioreactor

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*Abbreviations:* AnMBR, anaerobic membrane bioreactor; PAC, powder activated carbon; GAC, granular activated carbon; SRT, solids retention time; VFAs, volatile fatty acids; MBRs, membrane bioreactors; AC, activated carbon; DOM, dissolved organic matters; BAC, biologically activated carbon; EPS, extracellular polymeric substance; DMBR, aerobic dynamic membrane bioreactor; TMP, transmembrane pressure; COD, chemical oxygen demand; SMP, soluble microbial products; SMX, sulfamethoxazole; TC, tetracycline; ETS, erythromycin-tetracycline-sulfamethoxazole; ST, erythromycin-tetracycline; Tmp, trimethoprim; Cbz, carbamazepine; Dcf, diclofenac; Tcs, triclosan; DOC, dissolved organic carbon; EGSB, expanded membrane-coupled granular sludge bed; DIET, direct interspecies electron transfer; UASB, upflow anaerobic sludge blanket; LCWW, low-grade coal wastewater; ZVI, zero-valent iron; ORP, oxidation-reduction potential; MLSS, mixed liquor suspended solids; TP, total phosphorous; EGSB, expanded granular sludge bed; SCFA, short chain fatty acids; LCFA, long chain fatty acids; SS, suspended solid; AOX, adsorbable organic halogen

23 can effectively mitigate membrane fouling by altering the feed properties. Activated carbon,  
24 such as powdered activated carbon (PAC) and granular activated carbon (GAC), has been  
25 widely applied as an adsorbent to aerobic and anaerobic membrane bioreactors for membrane  
26 fouling control. Organic enhancers such as biochar and waste yeast, and inorganic enhancers  
27 like polyaluminum chloride and zeolite have also been applied to AnMBRs promoting  
28 flocculation and coagulation. Thus, this review discusses the impacts of different fouling  
29 reduction enhancers under anaerobic conditions as well as AnMBR system. In addition, the  
30 mechanisms of the enhancers mitigating the membrane fouling are also summarized for better  
31 understanding of the effects of the enhancers in AnMBRs.

32 **Keywords:** Anaerobic membrane bioreactor; membrane fouling; enhancers; activated carbon

33

## 34 **1. Introduction**

35 In recent years, anaerobic membrane bioreactor (AnMBR) technology, which combines  
36 anaerobic process and membrane filtration, has been gaining increasing popularity. AnMBRs  
37 have the same benefits as aerobic MBRs, such as a footprint reduction and superior permeate  
38 quality. AnMBRs also can provide several advantages over the aerobic processes, including  
39 long solids retention time (SRT), low sludge production and potential energy use [1].  
40 Moreover, as AnMBR is the integration of anaerobic digestion process with membrane  
41 separation, these processes can provide benefits as well. Anaerobic digestion process, which  
42 involves four major stages of hydrolysis, acidogenesis, acetogenesis and methanogenesis,  
43 occurs in the bioreactor. Throughout this process, organic materials are biodegraded into  
44 volatile fatty acids (VFAs) and hydrogen as intermediate products and into methane as a final  
45 product [2]. All these products can make the AnMBR an energy neutral or even energy positive  
46 technology. In addition, unlike anaerobic digestion that requires mesophilic ranges from 35°C

47 to 37°C, AnMBR can be operated in room temperature or even in cold temperatures by  
48 expanding SRT, which is both cost and energy-efficient [3].

49

50 However, there are some issues that need further attention in AnMBR technology. One of the  
51 most challenging issues is membrane fouling, which deteriorates the performance of membrane  
52 and shortens membrane lifespan. Membrane fouling generally occurs when the components of  
53 sludge interact with membrane material, causing an initial pore blocking and cake layer  
54 formation. It is reported that membrane fouling in AnMBR has more severe impacts compared  
55 to the aerobic system in terms of pollutant removal efficiency and sludge characteristics, even  
56 using the same membrane material [1]. Meng et al. [4] also mentioned that the cake layer  
57 formed with anaerobic sludge might have a comparatively lower removability than that with  
58 aerobic sludge.

59

60 Many researchers have carried out studies on alleviating membrane fouling, which have  
61 involved pretreatment of feed wastewater, optimization of operational conditions, membrane  
62 module or surface modification [1, 3, 5]. To control membrane fouling, different pretreatment  
63 methods have been introduced, such as alkaline pretreatment, acid pretreatment, ozone  
64 pretreatment and settling organic contaminants [6-9]. Some studies have shown that feed  
65 characteristics have significant impacts on the formation and compactness of the cake layer.  
66 Enhancers, such as adsorbent agents, carriers and other chemical agents, can be effective in  
67 modifying the properties of feed water in AnMBRs. Adsorbents, such as activated carbon,  
68 zeolite and bentonite, promote adsorption and ion exchange phenomena. Coagulants including  
69 polyaluminum chloride and ferric chloride, and suspended carriers can promote coagulation

70 and flocculation, respectively. Consequently, enlarged floc size and decreased soluble organics  
71 in the supernatant can mitigate membrane fouling [1, 10].

72 To date, there are many investigations of fouling control in aerobic MBRs by adding different  
73 additives as adsorbents [11, 12], coagulants/flocculants [13-16] and suspended carriers [17].  
74 However, only a limited amount of research is available to investigate the effects of enhancers  
75 on fouling control in anaerobic MBRs. Additionally, most review papers of fouling control in  
76 AnMBRs have only focused on controlling operating conditions and overall mitigation  
77 strategies [1, 5, 18, 19]. This is the first review article that focuses on the different kinds of  
78 fouling reduction enhancers in AnMBR and their influences on membrane fouling reduction.  
79 Effects of adding activated carbon including powdered activated carbon (PAC) and granular  
80 activated carbon (GAC) on AnMBR performance will firstly be discussed. Then the following  
81 sub-sections will concentrate on the effects of adding other enhancers.

82

## 83 **2. Enhancers to AnMBR**

### 84 **2.1 Activated carbon**

85 Activated carbon (AC) has been widely applied in membrane bioreactors (MBRs) due to its  
86 high adsorption capability, enhancement of biodegradation, and subsequent removal of  
87 recalcitrant pollutants. The addition of AC can also efficiently mitigate membrane fouling, as  
88 it has high potential to enhance membrane flux as well as removal performance of chemical  
89 oxygen demand (COD) and recalcitrant pollutants [20, 21]. Moreover, the use of AC in the  
90 anaerobic digestion process has been gaining more attention because it facilitated the  
91 alleviation of organic shock loading, the enrichment of essential anaerobic microorganisms and  
92 the improvement of anaerobic digestion stability [21].

93

94 There are two types of AC, namely PAC and GAC. PAC has high porosity and large surface  
95 area, which can lead to high adsorption capacity, while removing odour, colour and taste [21].  
96 Compared to PAC, GAC has larger size than PAC, which is more easily retained in the reactor  
97 and more economical when it is used continuously, because GAC can be regenerated by  
98 thermal process. Due to the larger size, GAC also has stronger physical interactions with the  
99 membrane surface [22].

100

### 101 **2.1.1 Powdered activated carbon**

102 PAC can reduce membrane fouling through three mechanisms. Firstly, at the initial stage of  
103 PAC addition, adsorption of organic matters occurs, which greatly removes the dissolved  
104 organic matters (DOM) from wastewater. Secondly, after initially adsorbing organic matters  
105 and becoming saturated, microorganisms aggregate on the porous surfaces of PAC particles as  
106 supporting medium for attached bacterial growth [23]. Finally, the formation of biologically  
107 activated carbon (BAC) promotes the degradation of pollutants and modifies the sludge  
108 properties, which is the most important mechanism. After the colonization of microorganisms,  
109 the planktonic microorganisms transform into biofilm. Once attached bacteria produce  
110 extracellular polymeric substance (EPS), it helps not only the attachment of microorganisms to  
111 biofilm, but also the stabilisation of the biofilm structure. The active biofilm continues to  
112 biodegrade organic compounds as well as to reduce the attachment of microorganisms on the  
113 membrane surface so that it can relieve the membrane biofouling [12, 24]. In addition, the  
114 scouring effect of PAC also alleviates membrane fouling, as it can remove the deposited cake  
115 layer on membrane surface while limiting the accumulation of foulants [25]. Figure 1 illustrates  
116 the mechanism of fouling reduction when activated carbon is added.

117

118 More recent studies have confirmed that PAC has positive effects on sludge morphology,  
119 aggregation ability of sludge flocs and microbial properties, and thus the pollutants removal  
120 mechanism can be enhanced. The study by Zhang et al. [26] reported that PAC addition in a  
121 submerged AnMBR was able to form larger floc size of the sludge compared to AnMBR  
122 without PAC. However, in case of long-term operation over 140 days, the sludge diameter  
123 decreased from 20.66  $\mu\text{m}$  to 17.00  $\mu\text{m}$ , which was contrary to the result from previous research  
124 about PAC in AnMBR [27]. This may have resulted from the fact that PAC enabled the  
125 generation of free living filamentous microbes after the long term operation and prevented the  
126 large floc size formation in mixed liquor. In addition, the sludge aggregation ability was able  
127 to be assessed using the total interaction energy which is a function of separation distance  
128 between the sludge surfaces. It could be calculated by summing Lifshitz-van der Waals energy,  
129 Lewis acid-base energy and repulsive or attractive electrostatic double layer energy [28, 29].  
130 PAC addition showed highly negative value of total interaction energy per unit area of sludge,  
131 which indicated that the characteristics of sludge surface has transformed into hydrophobicity,  
132 and thus sludge cells adherence could be strengthened by stronger attractive interaction. This  
133 improvement of aggregation ability led to more stable sludge flocs and potentially reduced the  
134 EPS release, which mitigated the pore blocking and irremovable membrane fouling [11]. The  
135 increased bacterial diversity and evolution of the bacterial community were also attributed to  
136 PAC addition creating additional microbial environment in the form of BAC, which promoted  
137 the enrichment and growth of some special functional bacteria. The enrichment of  
138 *Acinetobacter*, *Comamonas*, *Flavobacterium* and *Pseudomonas*, which can contribute to  
139 formation of sludge flocs and degradation of organics, were highly promoted [28]. When PAC  
140 was applied in anaerobic batch biofilm reactors as a biofilm carrier for the enhancement of  
141 refractory compounds degradation, it increased the abundance of *Methanothrix*,

142 *Methanomassiliicoccus*, and *Methanobacterium* which were favourable for the methane  
143 production [30].

144

145 In a study of Hu and Stuke [31], 1.7 g/L of PAC addition to submerged AnMBR showed  
146 significant benefits for the removal of fine colloidal particles as well as membrane flux  
147 improvement and transmembrane pressure (TMP) reduction. It was also found that PAC  
148 addition showed 22.4% of increase rate in COD removal, while GAC showed no significant  
149 increase. The reason why PAC was more efficient than GAC in terms of COD removal, might  
150 be due to the greater surface area per mass than GAC. Another study, which applied 1.7 g/L of  
151 PAC as well, showed 30% increased dissolved organic carbon (DOC) removal and decrease in  
152 SMP concentration [32]. On the other hand, when the more PAC concentration of 4 g/L was  
153 added, the SMP was rather accumulated while having excellent COD and colour removal  
154 efficiency [33, 34]. Several studies have revealed that the PAC addition not only decreased  
155 turbidity and colour, but also removed potential foulants such as fine colloids and soluble  
156 microbial products (SMP), which could lead to the reduction of fouling layer thickness [25, 26,  
157 35]. Table 1 summarizes the effects of PAC addition on membrane fouling control in  
158 submerged AnMBRs.

159

160 PAC can also be beneficial to AnMBRs in terms of the removal of antibiotics, which have  
161 negative impact on membrane fouling. In fact, the existence of antibiotics in AnMBRs has  
162 worsened performance and issues associated with membrane fouling, since it could lead to a  
163 decrease of the floc size and pH, and an increase in the secretion of EPS and SMP. Moreover,  
164 it could facilitate the development of microbial communities which had the most contribution  
165 to membrane fouling, such as *Firmicutes*, *Proteobacteria* and *Chloroflexi* [36, 37]. According

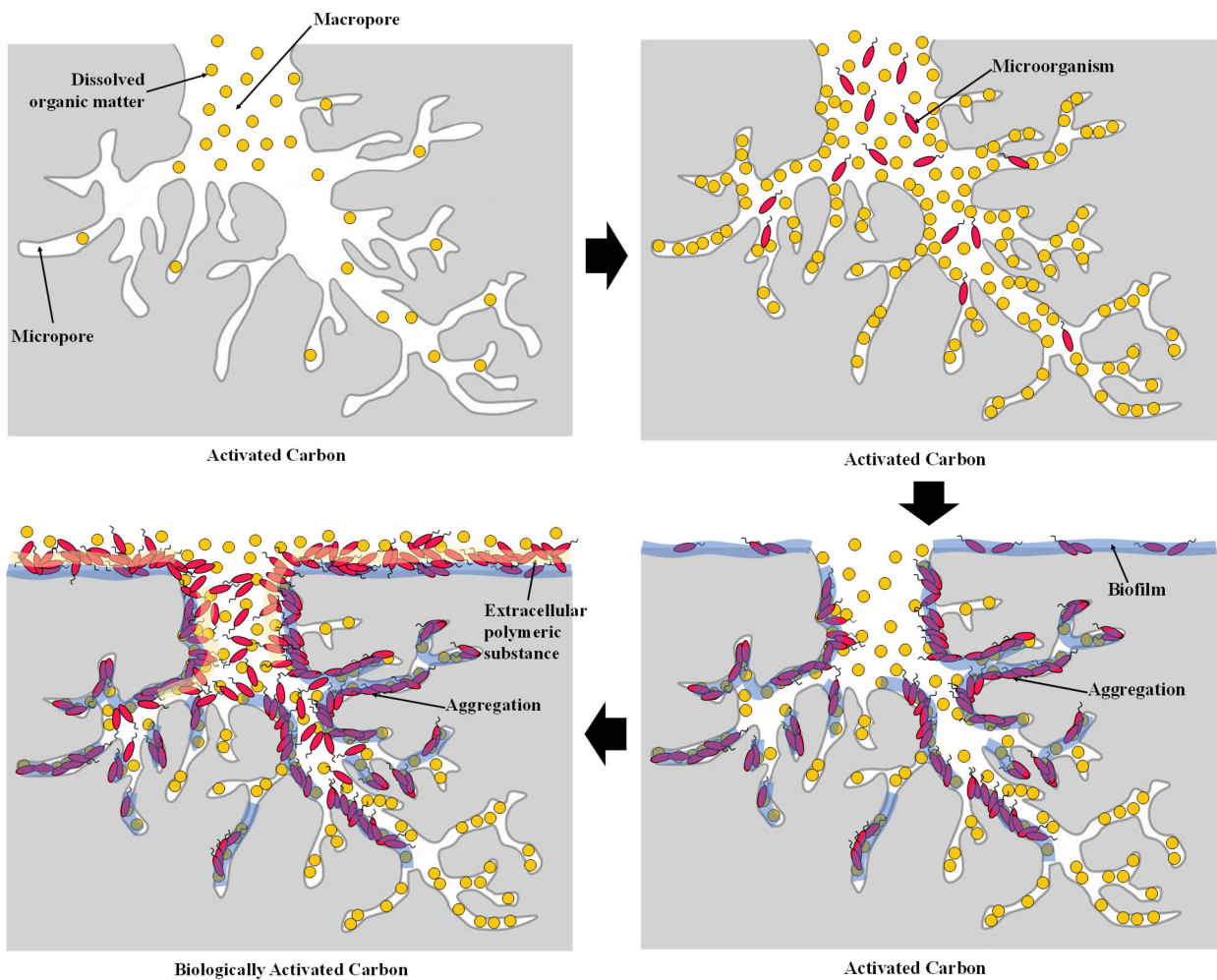
166 to a review by Cheng et al. [38], the addition of antibiotics and combined antibiotics to  
167 anaerobic reactors, such as sulfamethoxazole (SMX), tetracycline (TC), erythromycin-  
168 tetracycline-sulfamethoxazole (ETS), and erythromycin-tetracycline (ST), could cause  
169 negative effects on pH, COD removal efficiency, and biogas production. Both the pH value  
170 and COD removal efficiency in anaerobic sequencing batch reactors significantly decreased  
171 when the high concentration of antibiotics, such as 45 mg/L of SMX, 8.5 mg/L of TC, and 46  
172 mg/L of ETS, were added [39-41]. Biogas generation, which is inherently related to COD  
173 removals under anaerobic conditions, was inhibited as well, and the reason for this might be  
174 the methanogenesis process was sensitive to the presence of antibiotics in anaerobic processes.  
175 Likewise, 100 µg/L of SMX and TC in anaerobic/aerobic-MBR accelerated the rate of TMP  
176 rise and decreased the membrane fouling cycle from 25 days to 8 days. In addition, the fouling  
177 layer became denser and thicker with 20 µm of thickness. Furthermore, higher concentration  
178 of two antibiotics, 1000 µg/L of SMX and TC, resulted in further decrease in membrane fouling  
179 cycle to 4 days and 40 µm of the fouling layer thickness [42]. However, the addition of activated  
180 carbon could remediate these negative results. As a case in point, the addition of PAC into  
181 AnMBR increased removal efficiencies of five different pharmaceuticals including SMX,  
182 trimethoprim (Tmp), carbamazepine (Cbz), diclofenac (Dcf), and triclosan (Tcs) by  
183 approximately 5%-92%, as the adsorption of pharmaceuticals to PAC thermodynamically  
184 enhanced their biotransformation [43].

185

186 Although the optimal dosage of PAC resulted in significant alleviation in membrane fouling,  
187 overdosing might have contrary results due to its potential to become a foulant. Akram and  
188 Stuckey [44] proposed that appropriate amount of PAC should be added for the best  
189 improvement of performance of AnMBR and membrane fouling amelioration. In their



190 research, PAC concentration of 1.67 g/L highly improved the flux by more than four times,  
191 while 3.4 g/L of PAC caused a decrease of flux and adsorption incapacity of PAC to higher  
192 concentration of biomass. The excessive dosage of PAC could result in poor membrane  
193 filtration due to the increased sludge viscosity caused by the presence of more extracellular  
194 polymers. Moreover, small PAC particles (8-35  $\mu\text{m}$ ) at high concentration in suspension  
195 increased turbidity of mixed liquor and caused more membrane pore blockage and abrasion  
196 [20]. Therefore, the optimal PAC dosage is effective for flux improvement and adsorption of  
197 fine solutes, and regular replacement of aged PAC with fresh PAC is necessary [4].



198

199 **Figure 1.** Mechanism of fouling reduction performance of activated carbon

200 **Table 1.** Effects of PAC addition on performance of submerged AnMBRs

AC supplier	Dose of AC	Feed water	Operating conditions	Effects on performance <sup>a</sup>	References
<ul style="list-style-type: none"> <li>Norits-Super</li> <li>Total surface area of 1300 m<sup>2</sup>/g</li> </ul>	1.7 g/L	Saline sewage	<ul style="list-style-type: none"> <li>SRT : 250 d</li> <li>HRT : 8, 20 d</li> <li>OLR : 2 gCOD/L·d</li> <li>Flux : 5 - 8 L/m<sup>2</sup>·h</li> <li>Salinity : 0-35 gNaCl/L</li> <li>Temperature : 35 ± 1°C</li> </ul>	<ul style="list-style-type: none"> <li>Decrease in TMP by 0.070 bar</li> <li>Increase in dissolved organic carbon (DOC) removal by 30% in the reactor and 5% in effluent</li> <li>Reduction of high MW compounds by 70%</li> <li>Reduction of large flocs attached to the biofilm</li> <li>Decrease in SMP</li> </ul>	[32]
<ul style="list-style-type: none"> <li>Norit, Singapore</li> <li>BET surface area of 925 m<sup>2</sup>/g</li> <li>average particle size of 22 µm</li> </ul>	1 g/L	Synthetic sewage	<ul style="list-style-type: none"> <li>SRT : 213 d</li> <li>HRT : 6 h</li> <li>Flux : 5 L/m<sup>2</sup>·h</li> <li>Feed COD : ~500 mg/L</li> <li>Total nitrogen : ~100 mg/L</li> <li>Temperature : 35°C</li> </ul>	<ul style="list-style-type: none"> <li>Enhanced removal of five selected pharmaceuticals (Tmp, Smx, Cbz, Dcf, Tcs) by about 5-92%</li> <li>Increased biotransformation of Tmp by 4.5%, Smx by 18.8% and Tcs by 34.8%</li> </ul>	[43]
<ul style="list-style-type: none"> <li>Norit, UK</li> <li>Average particle size : 15-25 µm</li> </ul>	400 mg/L	Synthetic sewage	<ul style="list-style-type: none"> <li>Flux : 15 L/m<sup>2</sup>·h</li> <li>Feed COD : 500 mg/L</li> <li>VSS : 5.0-5.5 g/L</li> <li>Temperature : 35°C</li> <li>pH : 6 - 7</li> </ul>	<ul style="list-style-type: none"> <li>Reduction in supernatant supra-colloidal particles, colloids and SMPs</li> <li>Reduced thickness of fouling layer reduced</li> <li>Declined levels of COD by 13% and proteins</li> </ul>	[26]
<ul style="list-style-type: none"> <li>Norit, UK</li> </ul>	1.67, 3.4 g/L	Synthetic wastewater	<ul style="list-style-type: none"> <li>SRT : 250 d</li> <li>HRT : 6 h</li> <li>OLR : 16 gCOD/L·d</li> <li>Feed COD : 4 g/L</li> <li>Temperature : 35 ± 1°C</li> </ul>	<ul style="list-style-type: none"> <li>Enhanced performance during start-up period (i.e. shortened start-up duration, increased COD removal, declined SMP level,</li> </ul>	[44]

			<ul style="list-style-type: none"> <li>• Neutral pH</li> </ul>	<ul style="list-style-type: none"> <li>increased concentration of biomass and enrichment of microorganisms)</li> <li>• Adsorption of biodegradable low and high MW residual COD by PAC</li> <li>• Adsorption of fine colloids and dissolved organics by PAC</li> <li>• Improvement in flux (i.e, increase in flux from 2 to 9 L/m<sup>2</sup>·h with 1.67 g/L PAC)</li> </ul>	
• Synth®	4 g/L	Textile wastewater	<ul style="list-style-type: none"> <li>• HRT : 24 h</li> <li>• Temperature : 35°C</li> <li>• pH : 6.8 – 7.2</li> <li>• Feed COD : 670 mg/L</li> <li>• COD:N:P : 350:5:1</li> </ul>	<ul style="list-style-type: none"> <li>• Enhanced removals of COD, VFA, turbidity and colour by about 11%, 8%, 43% and 69%, respectively</li> <li>• Increased reactor stability</li> <li>• Enhanced membrane permeability (higher critical flux)</li> <li>• Adsorption of toxic compounds, aromatic amines and VFA by PAC</li> <li>• Increased accumulation of SMP</li> </ul>	[34, 35]
• Synth®	4 g/L	Domestic sewage	<ul style="list-style-type: none"> <li>• HRT : 24 d</li> <li>• COD:N:P : 350:5:1</li> <li>• OLR : 0.53 kg/m<sup>3</sup>·d</li> <li>• Temperature : 35°C</li> <li>• pH : 6.5 – 7.5</li> </ul>	<ul style="list-style-type: none"> <li>• Enhanced COD and colour removal</li> <li>• Increased reactor stability</li> <li>• Less accumulation of VFA</li> <li>• Adsorption of aromatic amines by PAC</li> </ul>	[33]
• Extra pure charcoal powdered activated carbon	1, 3, 5 g/L	Palm Oil Mill Effluent (POME)	<ul style="list-style-type: none"> <li>• SRT : 30 d</li> <li>• HRT : 6 d</li> <li>• Feed COD: 4.74 ± 1 g/L</li> <li>• Temperature : 35°C</li> <li>• pH : 7-8</li> </ul>	<ul style="list-style-type: none"> <li>• Increased COD removal efficiency</li> <li>• Increased floc size at higher PAC dosage</li> </ul>	[25]

- 
- At mesophilic condition
  - More reduction of EPS concentration and membrane fouling at higher PAC dosage
- 

201 <sup>a</sup>Cbz, carbamazepine; Dcf, diclofenac; Smx, sulfamethoxazole; TCS, triclosans; Tmp, Trimethoprim

## 202 2.1.2 Granular activated carbon

203 In recent years, the addition of GAC has been extensively applied in anaerobic digestion  
204 process to enhance both reactor efficiency and abundance of special functional  
205 microorganisms. Anaerobic digestion process contains electron exchange between  
206 fermentative bacteria and methanogens in the form of metabolites, such as acetate, H<sub>2</sub> and  
207 methanol. Previous studies have demonstrated that conductive additives like GAC enabled  
208 direct electron exchange instead of metabolites, which could eventually enhance methanogenic  
209 conversion of short-chain fatty acids, such as acetate, butyrate, and propionate, and subsequent  
210 improvement of methane production [45-47]. Zhang et al. [48] showed that GAC remarkably  
211 promoted methanogenesis by enhancing direct interspecies electron transfer between  
212 fermentative bacteria, *Geobacteraceae*, and methanogens, *Methanosaetaceae*. Another  
213 research has also concluded that surface modified GAC with magnetite stimulated enrichment  
214 of electroactive bacteria, such as *Shewanella*, *Pseudomonas*, *Geobacter* and *Desulfuromonas*,  
215 enhancing the methane production by a degradation of propionate to acetates and electrons that  
216 can be utilized by methanogens [45].

217

218 As a membrane fouling mitigation strategy, methods of inducing unsteady-state shear on the  
219 membrane surface, such as bubbling and vibration, have been applied to MBRs. Particle  
220 fluidization recently has been presented as an alternative to bubbling, as it could have the same  
221 effect on membrane fouling reduction with at least ten times lower energy requirements than  
222 bubbling. Particularly, the fluidization of GAC has gained significant attention, because larger  
223 GAC was more effective during long-term operation [49, 50]. Therefore, previous studies have  
224 reported that GAC fluidization resulted in significant membrane fouling alleviation in  
225 anaerobic fluidized membrane bioreactor [51-56]. In the studies of integrated anaerobic

226 fluidized-bed membrane bioreactor, high amount of protein was adsorbed resulting in  
227 remarkable improvement of membrane filtration [52, 53]. The effect of GAC fluidization has  
228 been demonstrated with its energy efficient and effective advantages, unlike the popular air-  
229 sparging method which required comparatively high energy costs [57]. As GAC fluidization is  
230 one way to induce unsteady-state shear on membrane, which has been identified as a cost-  
231 effective method, it could reduce the energy requirement in the process [58]. As a case in point,  
232 the electrical energy requirement for anaerobic fluidized-bed ceramic membrane bioreactor  
233 operation was estimated to be 0.039 kWh/m<sup>3</sup>, which was only 17% of electrical energy that  
234 can be generated from produced methane [59]. The average energy consumption of GAC  
235 fluidization is generally reported as 0.15 kWh/m<sup>3</sup>, whereas that of gas sparging is twice higher,  
236 which is 0.31 kWh/m<sup>3</sup> including pumping and mixing [60]. The table 2 summarizes the effects  
237 of GAC in anaerobic fluidized membrane bioreactor.

238

239 In the research of Ding et al. [61], they added 50 g/L of GAC to an expanded membrane-  
240 coupled granular sludge bed (EGSB) and showed a remarkable enhancement of COD removals  
241 (80% vs 62% without PAC) and decrease in SMP concentration. The cake layer resistance,  
242 which was the main fouling mechanism in membrane-coupled EGSB process, was also  
243 decreased by 53.5%. Another research by Wang et al. [62] treating wastewater containing  
244 phenol and quinolone reported that a 2 g/L of GAC could not only remove COD and SMP by  
245 adsorption, but also enhance the degradation of phenol and quinolone. The high adsorption  
246 capacity of GAC could capture some fouling-causing compounds like SMP prior to attachment  
247 on membrane surface. Meanwhile, GAC could scour the foulants from the membrane surface  
248 and prevent the accumulation of foulants. Hence, the use of GAC as suspended medium  
249 effectively mitigated irreversible fouling [63]. As a case in point, the scouring effect of GAC

250 with flux of 16 L/m<sup>2</sup>·h in a two-stage anaerobic fluidized membrane bioreactor was able to  
251 mitigate membrane fouling, along with effective removal of 20 commonly found  
252 pharmaceuticals (i.e. ibuprofen, caffeine, and SMX, etc.) through adsorption and  
253 biodegradation [64, 65].

254

255 Although having positive effects on membrane fouling control, Wu et al. [55] suggested that  
256 the behaviour and characteristics of GAC might have a harmful influence on membrane  
257 performance. Due to the fine carbon particles that are released from GAC itself during  
258 fluidization, the fouling could be aggravated by blocking the pores and forming a thin cake  
259 layer. GAC abrasion also led to a partial loss from the initial membrane quality. The reduction  
260 in adsorption capacity of GAC over time was also a major limitation. Thus, the exhausted GAC  
261 needs to be replaced or regenerated by thermal process to recover the adsorption capability  
262 [24].

263

264 Furthermore, the energy requirements for fluidization and membrane fouling mitigation were  
265 significantly different depending on the particle size of GAC as well as adsorption capacity.  
266 When the adsorption of fresh GAC predominantly took place, comparatively small GAC  
267 particles had greater effect on fouling reduction due to large surface area, along with less energy  
268 consumption. However, after the adsorption capacity was exhausted, dominant process for  
269 fouling reduction became the scouring effect. Then, the relatively large GAC particles were  
270 more effective in fouling reduction, but more energy is required for fluidization [66]. Charfi et  
271 al. [67] showed that 2-3 mm of GAC particles acted as a better method of fouling reduction by  
272 removing cake layer on membrane surface, whereas small particles from 0.18 mm to 0.5 mm  
273 rather intended to accumulate on membrane surface. It was also found that, although large

274 particles were more effective in scouring due to inertial forces, the energy requirement on  
275 fluidizing the particle was also higher [49]. Thus, further studies are necessary for a better  
276 understanding of production of fine carbon particles, GAC abrasion and choosing suitable  
277 particle sizes for mitigating membrane fouling.



Performance of fluidized AnMBRs

Feed water	Operating condition	Effects of GAC on performance	References
Primary-settled domestic wastewater	<ul style="list-style-type: none"> <li>• SRT : 485 d</li> <li>• HRT : 4.5 – 6.8 h</li> <li>• Temperature : 8 - 30 °C</li> <li>• Average effluent COD : ~23 mg/L</li> </ul>	<ul style="list-style-type: none"> <li>• No chemical membrane cleaning</li> </ul>	[54]
Synthetic wastewater	<ul style="list-style-type: none"> <li>• HRT : 8.7 h</li> <li>• Feed COD: 150 mg/L</li> <li>• Flux : 5 L/m<sup>2</sup>·h</li> <li>• Temperature : 25 °C</li> </ul>	<ul style="list-style-type: none"> <li>• Complete removals of diclofenac, ibuprofen and sulfamethoxazole</li> </ul>	[64]
Municipal wastewater primary-clarifier effluent	<ul style="list-style-type: none"> <li>• HRT : 2.3 h</li> <li>• Flux : 6 - 11 L/m<sup>2</sup>·h</li> <li>• OLR : 1.0 – 3.5 kgCOD/m<sup>3</sup>·d</li> <li>• Temperature : 25 °C</li> </ul>	<ul style="list-style-type: none"> <li>• No requirement of other fouling control process</li> <li>• Lower electrical energy requirements</li> </ul>	[56]
Domestic wastewater	<ul style="list-style-type: none"> <li>• HRT : 1.3 – 2.1 h</li> <li>• Feed COD: 250 mg/L</li> <li>• Flux : 22 L/m<sup>2</sup>·h</li> <li>• Temperature : 25 °C</li> <li>• pH : 7.3 -7.6</li> </ul>	<ul style="list-style-type: none"> <li>• Lower biosolids production</li> <li>• Low energy requirement (10% of energy converted form methane)</li> </ul>	[51]
Dilute wastewater	<ul style="list-style-type: none"> <li>• HRT : 1.3 – 2.1 h</li> <li>• Feed COD: 300mg/L</li> <li>• Flux : 22 L/m<sup>2</sup>·h</li> </ul>	<ul style="list-style-type: none"> <li>• Lower energy requirement</li> <li>• No adverse effect of</li> </ul>	[59]

Two-stage AnFMBR	<ul style="list-style-type: none"> <li>• 10 × 30 mesh</li> <li>• Bulk density: 500–1000 m<sup>2</sup>/g</li> <li>• specific gravity: 0.85 and 2 g/cm<sup>3</sup></li> <li>• 25% in AFBR, 50% in AFMBR</li> </ul>	Municipal wastewater	<ul style="list-style-type: none"> <li>• HRT : 1.28 h</li> <li>• OLR : 5.65 kgCOD/m<sup>3</sup>·d</li> <li>• Feed COD: 250mg/L</li> </ul>	<ul style="list-style-type: none"> <li>• Effective removals of pharmaceuticals</li> <li>• No requirement of other fouling control process</li> </ul>	[65]
AnFMBR	<ul style="list-style-type: none"> <li>• &gt;2mm,</li> <li>• 0.85-2mm</li> <li>• 0.5-0.85mm</li> <li>• 0.18-0.5mm</li> <li>• &lt;0.18mm</li> <li>• 10%, 30%, 50%</li> </ul>	Synthetic wastewater	<ul style="list-style-type: none"> <li>• Flux : 50 L/m<sup>2</sup>·h</li> <li>• Feed COD: 250 mg/L</li> </ul>	<ul style="list-style-type: none"> <li>• Energy requirement increased with particle size</li> <li>• The higher the packing ratio, the greater the fouling reduction</li> </ul>	[66]
AnFMBR	<ul style="list-style-type: none"> <li>• N/A</li> </ul>	Screened domestic wastewater	<ul style="list-style-type: none"> <li>• SRT : 12 d</li> <li>• HRT : 4 h</li> <li>• Flux : 7.6- 7.9 L/m<sup>2</sup>·h</li> <li>• OLR : 1.3 -1.4 kgCOD/m<sup>3</sup>·d</li> <li>• Temperature : 13 - 32°C</li> </ul>	<ul style="list-style-type: none"> <li>• Similar BOD<sub>5</sub> and COD removal efficiencies (around 85%) achieved when operating at a 65% shorter HRT than gas-sparing system (removals of around 90%)</li> </ul>	[60]
AnFMBR	<ul style="list-style-type: none"> <li>• Lignite coal (0.42-0.85mm, 650 m<sup>2</sup>/g)</li> <li>• Peat bog (0.85-2.4mm, 600-800 m<sup>2</sup>/g)</li> </ul>	Synthetic wastewater	<ul style="list-style-type: none"> <li>• Flux : 14 L/m<sup>2</sup>·h</li> </ul>	<ul style="list-style-type: none"> <li>• Fouling reduction and detrimental effects on membrane</li> </ul>	[55]

	<ul style="list-style-type: none"> <li>• Peat bog (2.4-4.6mm, 600-800 m<sup>2</sup>/g)</li> </ul>			
IAFMBR	<ul style="list-style-type: none"> <li>• 40g</li> <li>• 10 × 30 mesh</li> </ul>	Domestic wastewater	<ul style="list-style-type: none"> <li>• HRT : 6 h</li> <li>• Flux : 7.1 L/m<sup>2</sup>·h</li> <li>• Feed COD: 247 - 449 mg/L</li> <li>• Permeation : 23.2 L/d</li> <li>• Temperature : 35, 25, 15 °C</li> <li>• pH : 7.18 – 7.99</li> </ul>	<ul style="list-style-type: none"> <li>• High protein adsorption by GAC</li> </ul>
IAFMBR	<ul style="list-style-type: none"> <li>• 200 -300g</li> <li>• 10 × 30 mesh</li> </ul>	Domestic wastewater	<ul style="list-style-type: none"> <li>• HRT : 4, 6, 8 h</li> <li>• Flux : 0.27 m<sup>3</sup>/m<sup>2</sup>·d</li> <li>• Feed COD: 300 mg/L</li> <li>• Temperature : 35 ± 2°C</li> <li>• pH : 7.5 ± 0.21</li> </ul>	<ul style="list-style-type: none"> <li>• Adsorption of protein in cake layer by GAC</li> <li>• Improved membrane filtration</li> </ul>

279  
280

<sup>a</sup>AFCMBR, anaerobic fluidized bed ceramic membrane bioreactor; AnFMBR, anaerobic fluidized membrane bioreactor; SAF-MBR, staged anaerobic fluidized membrane bioreactor; IAFMBR, integrated anaerobic fluidized-bed membrane bioreactor; SAF-CMBR, staged anaerobic fluidized bed ceramic membrane bioreactor.

## 281 **2.2 Other enhancers**

### 282 **2.2.1 Biochar**

283 Biochar is a porous and carbonaceous residue obtained from thermal decomposition of biomass  
284 in an oxygen deleted environment, or from other processes such as pyrolysis, hydrothermal  
285 carbonisation, gasification and torrefaction. It is usually produced at a lower temperature than  
286 700 °C, because reaction above 900 °C causes the destruction of walls between pores, which  
287 results in widening of pores of biochar [68, 69]. Unlike AC, it is produced without any  
288 activation, and this non-activation makes the specific surface area of biochar less efficient  
289 compared to AC. However, the production cost of biochar is one tenth cheaper than that of AC  
290 [68, 69, 71]. After a series of reactions of biomass such as dehydration, depolymerisation and  
291 carbonisation during thermal decomposition, three products, namely condensable liquid (bio-  
292 oil), non-condensable gases (syngas) and biochar are produced, which depends on the type of  
293 biomass used and process conditions (i.e. temperature and residence time). Biochar usually  
294 consists of fixed carbon, labile carbon and other volatile compounds, as well as moisture and  
295 ash. Fast pyrolysis aims at liquid oil production, whereas the goal of slow pyrolysis is biochar  
296 production, as the slow evaporation of water and release of volatile components can result in  
297 an increase in relatively fixed carbon content of the solid [70, 72]. The heterogeneous surface  
298 of biochar, which has both carbonised and non-carbonised fractions, accommodates several  
299 adsorption mechanisms. Physical adsorption, surface precipitation and the pore-filling are the  
300 major routes of adsorption. Moreover, for positively charged organic compounds, hydrophobic  
301 effect and hydrogen bonding of biochar surface are the important adsorption routes. On the  
302 other hand, the removal of inorganic compounds largely depends on electrostatic attraction,  
303 precipitation and ion exchange [70, 73].

304

305 The addition of biochar on anaerobic digestion process has shown to be effective in terms of  
306 biogas production and selectively enriched microbial groups. The biochar addition was able to  
307 enhance VFA production and degradation, and improve both hydrogen and methane production  
308 [68, 74]. Some studies demonstrated that better biogas production could be obtained from  
309 enhanced direct interspecies electron transfer (DIET) process by enrichment of electrogenic  
310 *Geobacter* and *Bacteroidetes*, which are potential direct interspecies electron transfer partners  
311 during anaerobic digestion [75, 76]. In addition, since biochar contains redox active moieties  
312 such as quinines, phenolics and phenazines, they can catalyse the electron transfer between  
313 biochar and outer membrane cytochromes during redox reactions [77, 78]. Moreover, biochar  
314 addition significantly enhanced methanogenesis by facilitating the enrichment of  
315 *Methanosarcina* even in high ammonium stress, and also favoured anaerobic sludge  
316 granulation, due to the ability of promoting biofilm formation and reducing the inhibition  
317 behaviour of ammonia [79, 80]. Similar to the biogas yield enhancement, biochar could  
318 facilitate hydrogen production via enrichment of hydrogen-producing bacteria [81]. The  
319 alleviation of sulphide toxicity during anaerobic treatment of sulphate-rich wastewater using  
320 biochar was investigated and biochar promoted reactor stability by adsorption of H<sub>2</sub>S from  
321 biogas [82]. Due to the adsorption capability and functional groups on the surface, biochar was  
322 also able to adsorb EPS and enhance sludge granulation, which could lead to significant  
323 mitigation of membrane fouling in aerobic MBRs [83-85].

324

325 Some previous studies have demonstrated that biochar could be beneficial to anaerobic  
326 membrane bioreactor. Bamboo charcoal, one kind of biochar, was able to enhance the removal  
327 performance of AnMBR as well as mitigate membrane fouling. In this study, two AnMBRs  
328 treating bamboo industry wastewater were analysed with and without bamboo charcoal  
329 addition. The result showed that COD removal efficiency increased about 5% after the addition

330 of bamboo charcoal, as well as reduced membrane fouling owing to the decrease of both SMP  
331 concentration and resistance of the fouling layer. Meanwhile, the methane yield became higher  
332 as a result of greater microbial activity of dominant microorganisms in methane production,  
333 such as *Methanosaeta*, *Methanospirillum* and *Methanobacterium*, occurring additionally inside  
334 the pores of the bamboo charcoal [86]. More recent study showed that membrane fouling was  
335 effectively reduced in a biochar-amended AnMBR along with 56% of decreased TMP rising  
336 rate and decreased proteins of EPS. In addition, *Arcobacter*, one of the bio-foulants that is  
337 involved in membrane biofouling, was hardly accumulated due to the presence of biochar [87].

338

### 339 **2.2.2 Waste yeast**

340 Waste yeast is traditionally used as a protein supplement in animal feed or alimentary substrate  
341 for the food processing industry. The brewing industry is the major source of spent yeast, which  
342 also produces other residues in addition to brewery wastewater, such as methanogens and small  
343 cellulosic particles [88]. Due to the high degradation capacity of yeast, it was favourable in  
344 treatment of landfill leachate, which contained high amount of recalcitrant compounds like  
345 phenolic compounds as well as toxic substances such as halogenated and heavy metals [89].  
346 Yeast had lower tendency to adhere on membrane surfaces than other microorganisms, so that  
347 its application in MBR can be beneficial in membrane fouling control and system operation  
348 [89]. The presence of yeast in aerobic MBR could significantly remove not only COD, colour  
349 and EPS, but also refractory substances including polyacrylamide [90-93].

350

351 Anaerobic co-digestion, which balances the nutrient component of different residues, is widely  
352 applied as a way to dilute potential toxic compounds and enhance biogas production [94]. Some  
353 previous studies have demonstrated that additional co-substrates in anaerobic wastewater

354 treatment increased methane production by maintaining a pH level within the methanogenesis  
355 range between 7.0 and 7.5, while improving the degradation of low biodegradable substrates  
356 [88, 95-97]. The research on the supplementation of yeast in brewery wastewater treatment as  
357 a co-substrate in a upflow anaerobic sludge blanket (UASB) reactor showed enhanced biogas  
358 production by 50%, while no significant changes in COD removal efficiency and accumulation  
359 of VFAs were observed up to 1.1 (v/v)% of brewery yeast concentration [88, 94]. These results  
360 indicated that the additional waste yeast could be a feasible substrate in anaerobic digestion in  
361 terms of high biodegradability and biogas yield.

362

363 The supplementation of yeast wastes as co-substrate in an AnMBR can have positive effects  
364 on membrane fouling control as well. A research by Yun et al. [98] investigated the effects of  
365 yeast on AnMBR performance treating low-grade coal wastewater (LCWW). Compared to no  
366 methane production in the absence of yeast wastes, AnMBR with yeast wastes gradually  
367 increased COD removal efficiency as well as methane production. In addition, the presence  
368 of yeast wastes showed the significant growth of some microorganisms such as  
369 *Methanococcus* and *Methanosarcina* which were responsible for the degradation of LCWW  
370 and biogas production. However, due to the metabolism of these bacteria, the fraction of  
371 SMPs and aromatic group with high molecular weight ( $> 1$  kDa) also increased. Thus, the  
372 addition of yeast wastes could be a potential alternative as an additive to AnMBR due to their  
373 positive effects on biodegradation of LCWW and growth of microorganisms, but further  
374 research should be carried out to find out the effect on fouling control.

375

### 376 **2.2.3 Iron**

377 Iron, which is the most abundant transition metal on the Earth, is also an essential component  
378 for the growth of most living organisms. Although iron itself is a non-toxic and electron donor  
379 in redox reactions, the presence of iron in anaerobic environment plays an important role in the  
380 electron cycling and metabolic activity of microorganisms [99, 100]. The Fe(II) and Fe(III),  
381 which are generated from several iron compounds, can be provided as nutrients for microbial  
382 activity or as redox mediators to facilitate the conversion of organic matters to methane [100].  
383 One of the strong reductants, zero-valent iron (ZVI), is an active anode material in  
384 electrocoagulation, and electrically produces Fe(II) ions which promote coagulation and  
385 effectively decrease the soluble and colloidal particular matters. Although the generation of  
386 Fe(II) ions from ZVI in aerobic process needs to be triggered by the electric field, it can occur  
387 spontaneously in the anaerobic digestion process. The protons, which are released by acidogens  
388 during the acidification, can help spontaneous generation of Fe(II) ions without any drive of  
389 electric field [101].

390

391 Many previous studies have investigated the addition of iron or ZVI into anaerobic digestion  
392 which could significantly increase methane production and improve COD removal [102-105].  
393 When iron was added to anaerobic aquatic environment, hydrogen was produced by iron  
394 corrosion. This hydrogen evolution can benefit methane production by enhancing both  
395 hydrogenotrophic methanogenesis and homoacetogenesis. In addition, iron was able to serve  
396 as an electron donor to reduce oxidation-reduction potential (ORP), and led to the decrease in  
397 propionic-type fermentation and subsequent enhancement of methanogenesis. As the  
398 accumulation of propionate destroyed the pH balance between acidogenesis and  
399 methanogenesis as well as hindered the methanogenesis of acetate, it should be reduced during  
400 the anaerobic process [106, 107]. Although anaerobic digestion can be limited by low



401 efficiency of hydrolysis and acidification, ZVI could intensify the activities of enzymes related  
402 to hydrolysis and acidification, such as protease which is responsible for catalysing hydrolysis  
403 of polysaccharide to monoses [107]. Moreover, the presence of ZVI stimulated the growth of  
404 hydrogen-consuming microorganisms such as homoacetogens and hydrogenotrophic  
405 methanogens, thereby enhancing acetate or methane production [107, 108]. In addition, iron  
406 could also effectively eliminate odorous H<sub>2</sub>S gas by precipitation of FeS. Likewise, the iron  
407 might be used for phosphate recovery in the form of compounds of iron and phosphate such as  
408 vivianite [99]. It was also found that the supplementation of iron salts to anaerobic digestion  
409 could be potentially advantageous to membrane fouling by supporting granulation and  
410 stabilisation. When ferrous iron was supplied to UASB reactor, anaerobic bacteria and EPS  
411 tended to adhere to iron in order to form a more stable structure with 56% of enlarged granule  
412 diameter. Moreover, inorganic precipitates such as ferrous sulphide could contribute to the  
413 stability of granules [109, 110].

414

415 The iron addition to AnMBR provided remarkable benefits on membrane fouling mitigation in  
416 several previous studies. Dong et al. [111] showed the influence of FeCl<sub>3</sub> as an additive in long-  
417 term operation of an AnMBR treating municipal sewage. The performance of the AnMBR,  
418 including removal efficiencies of COD and BOD<sub>5</sub>, was enhanced by adding 26 mg/L of FeCl<sub>3</sub>.  
419 Furthermore, even though the addition of FeCl<sub>3</sub> caused the increase of mixed liquor suspended  
420 solids (MLSS) concentration and formation of a more thickened cake layer, membrane fouling  
421 has been mitigated due to the more porous cake layer formation and increased filterability of  
422 mixed liquor. Zhang et al. [26] also investigated the addition of FeCl<sub>3</sub> to AnMBR, which  
423 effectively reduced membrane fouling by increasing both sludge floc size and the colloids as  
424 well as decreasing SMPs. Since iron remained in the reactor as a precipitate, resulting in

425 minimal concentration of iron in the effluent or supernatant, it was expected to be advantageous  
426 for a long term operation. In a recent study, ZVI has been applied into AnMBR with and  
427 without electric field. Although ZVI with electric field facilitated the increase of iron releasing  
428 rate of ZVI by 12 times and enhanced removal performances of COD and total phosphorous  
429 (TP) by about 3% and 50%, respectively, it resulted in more severe fouling due to the high  
430 density of Fe-rich fouling layer. However, ZVI without electric field significantly mitigated  
431 membrane fouling rate by 20% through the enhancement of mixed liquor filterability [101].

432

#### 433 **2.2.4 Calcium**

434 Calcium can be another special additive to alleviate fouling and enhance characteristics of  
435 granular sludge by enhancing bioflocculation. EPS, which is known to be the main substance  
436 affecting membrane fouling, typically contains negatively charged functional groups such as  
437 hydroxyl and carboxyl. Due to negatively charged EPS, cations play an important role in sludge  
438 flocculation. Divalent cations including calcium ions tend to combine preferentially with  
439 carboxylic functional groups of EPS and form bridges between the EPS molecules. This bridge  
440 formation promotes the improvement of bioflocculation, enlarges flocs and mitigates fouling  
441 [112-115]. Since the cost of calcium salts is relatively low, they have been widely used in  
442 aerobic process as an additive, which improve the properties of mixed liquor [114, 116].  
443 However, the decline in permeability and subsequent inorganic fouling occurred with high  
444 concentration of calcium of 830 mg/L, due to the precipitation of calcium carbonate. Therefore,  
445 more research is necessary to have a better understanding of effects of calcium addition and  
446 find out the optimal calcium concentration [117].

447

448 The addition of calcium can also positively affect anaerobic processes. Some previous studies  
449 have been conducted to evaluate the influence of calcium addition and the most effective  
450 dosage for anaerobic digestion. When five different concentrations of calcium chloride (CaCl<sub>2</sub>),  
451 which are 0, 1, 3, 5, and 7 g/L, were added to anaerobic digestion process, 3 g/L of calcium  
452 concentration was optimal for the best performance of anaerobic digestion and biogas  
453 production [118]. Similarly, according to a study of Ahmad et al. [119], calcium oxide (CaO)  
454 in the UASB reactor enhanced granulation and the accumulation of biomass as well as the  
455 degradation of butyrate and acetate acid. Since the addition of calcium on anaerobic digestion  
456 process significantly increased the abundance of *Methanosaeta* as the dominant methanogen,  
457 the methane production could be improved [120]. However, an overdose of calcium from 5 to  
458 7 g/L of concentration, which may lead to precipitation and limit mass transfer between  
459 microbes and organic compounds, further inhibit anaerobic process. When the precipitates such  
460 as calcium carbonate were formed on the surface or within the granules, they can cause sludge  
461 washout, as well as the declined methanogenic activity and diffusion limitation [118, 119].

462

463 Due to the positive effects of calcium addition on anaerobic process, the use of calcium as an  
464 additive in membrane bioreactors can also be a promising way to reduce membrane fouling  
465 [121]. An investigation on the effects of calcium addition (0, 50 and 100 mg/L of calcium) was  
466 conducted in three sequencing batch reactors with external dead-end microfiltration. The result  
467 showed that the highest dosage of calcium was able to enhance the reduction of fine particles,  
468 EPS and colloids in supernatant, leading to the mitigation of membrane fouling [122]. This  
469 significant reduction of membrane fouling was mainly due to calcium promoted  
470 bioflocculation, which achieved high volumetric organic removal and increased methane  
471 production rate. Furthermore, the enlarged size of anaerobic sludge granules by calcium

472 addition was also reported in some studies using membrane-coupled expanded granular sludge  
473 bed (EGSB) reactor or UASB reactors [123-126]. When calcium chloride was added to the  
474 EGSB reactor, the membrane fouling was alleviated effectively and the concentration of SMP  
475 decreased [121].

476

### 477 **2.2.5 Polyaluminum chloride**

478 One of the aluminum salts, polyaluminum chloride, generally consists of various polynuclear  
479 aluminum hydrolysis products, including Al monomers such as  $\text{Al}(\text{OH})^{2+}$ , dimer  $(\text{Al}_2(\text{OH})_2^{4+})$ ,  
480 trimer  $(\text{Al}_3(\text{OH})_4^{5+})$ ,  $\text{Al}_{13}(\text{AlO}_4\text{Al}_{12}(\text{OH})_{24}(\text{H}_2\text{O})_{12}^{7+})$  and aluminum hydroxide  $(\text{Al}(\text{OH})_3)$ . Due  
481 to the presence of these products, polyaluminum chloride is superior to the traditional  
482 aluminum coagulants, such as  $\text{AlCl}_3$  and  $\text{Al}_2(\text{SO}_4)_3$ , for removing organic matters [127]. The  
483 behaviour of aluminum coagulants can be greatly affected by basicity values ( $B$ ), which is the  
484 molar ratio of  $\text{OH}/\text{Al}^{3+}$ , because the dominant hydrolysis products are different under different  
485 basicity conditions. Polyaluminum chloride with high basicity value ( $B = 2.4$ ) resulted in  
486 increased membrane fouling propensity, as well as higher DOC removal efficiency and zeta  
487 potential of flocs, compared to polyaluminum chloride with lower basicity ( $B = 2.0$  and  $B =$   
488  $1.6$ ). This phenomenon might be related to the different dominant mechanisms of coagulation  
489 according to the content of Al species. As the percentage of  $\text{Al}_{13}$  increased along with the  
490 basicity value increase, it could provide a larger amount of positive charges for charge  
491 neutralization rather than adsorption bridge effect. As the flocs produced from charge  
492 neutralization are smaller than those from adsorption bridge effect, it could result in more  
493 severe membrane fouling [128].

494

495 Many previous studies have reported high charge neutralization capacity of polyaluminum  
496 chloride, which can lead to enlarged floc size and better filtration performance. The dose of  
497 polyaluminum chloride and subsequent hydrolysis can provide positive charge, which can  
498 neutralize the negatively charged sludge flocs and colloids. This neutralization results in  
499 weaker repulsion among flocs and colloids, and easier formation of large particles. In addition,  
500 SMP and EPS in mixed liquor can be compressed and removed from membrane surface by the  
501 charge neutralization and adsorption of polyaluminum chloride [129]. When polyaluminum  
502 chloride was added in anaerobic digestion process, it facilitated the reduction of SMP and  
503 improved sludge filterability. However, a high concentration of polyaluminum chloride over  
504 500 mg/L in anaerobic digestion could inhibit short chain fatty acids (SCFA) production as  
505 well as anaerobic process such as hydrolysis, acidogenesis and methanogenesis by decreasing  
506 the ratio of bioavailable nutrient, especially phosphorous [130, 131].

507

508 The positive effects of polyaluminum chloride dosing into AnMBR as an inorganic coagulant  
509 on membrane fouling control have been studied in some previous research. The addition of  
510 polyaluminum chloride could influence microbial characteristics as well as cake layer structure  
511 in the anaerobic digestion process. The abundance of anaerobic microorganisms, especially  
512 *Cloacimonetes* and *Smithella*, was significantly enriched in AnMBR [132]. Moreover,  
513 polyaluminum chloride was able to increase the hydrogen yield by washing out hydrogen  
514 consumers, including *Acetoanaerobium* and *Desulfobulbus* [127]. It was also reported that the  
515 cake layer on the membrane surface became more porous and looser when polyaluminum  
516 chloride was added, which could provide better filterability. A result from a study showed that  
517 polyaluminum chloride dosing could lower the composition rate of carbohydrate in SMP and  
518 EPS, as well as compress the concentration of EPS. This resulted in reduction of adherence

519 capacity of sludge and more substantially porous cake layer [129, 133].

520

### 521 **2.2.6 Zeolite**

522 Zeolite is a porous substance with high crystallinity, which mainly consists of aluminium,  
523 oxygen, and metals such as titanium, tin, and zinc. While natural zeolite can be normally found  
524 in rocks near volcanoes all over the world, it can also be synthesized or modified in order to  
525 improve properties for different applications. Both natural and modified zeolites can be used  
526 for adsorption and ion exchange. The presence of cations like  $\text{Na}^+$ ,  $\text{Ca}^{2+}$ ,  $\text{K}^+$  and  $\text{Mg}^{2+}$  on the  
527 porous surface of zeolite facilitates ion exchange from a contact solution. Thus, the use of  
528 zeolite can be applied in both aerobic and anaerobic biological processes including nitrification  
529 and denitrification, activated sludge, and anaerobic digestion. In aerobic processes, zeolite can  
530 act as an ion exchanger as well as a biomass carrier, whilst in anaerobic processes, zeolite can  
531 also act as an inhibitor of ammonia and heavy metals by ion exchange [134-136].

532

533 Zeolite has been reported to improve the performance of anaerobic processes as a porous  
534 microbial carrier as well as ion-exchanger. Its high ion-exchange capacity can contribute to  
535 enhance  $\text{NH}_4^+$  removal which is known as an inhibitor of anaerobic digestion. Indeed, Lin et  
536 al. [137] used modified zeolite to reduce  $\text{NH}_4^+$  concentration by ion exchange with  $\text{Na}^+$  and  
537  $\text{Ca}^{2+}$  as dominant ions for  $\text{NH}_4^+$  adsorption. Additionally, the application of zeolite also showed  
538 remarkable improvement in methane production and COD removal [138-140]. These  
539 improvements of anaerobic digestion can be attributed to ion exchange of  $\text{NH}_4^+$ , cations like  
540  $\text{Ca}^{2+}$  and  $\text{Mg}^{2+}$  and long chain fatty acids (LCFA) [140, 141]. Another researcher focused on  
541 the microbial communities apart from ion exchange, and suggested that zeolite could

542 specifically preserve the growth and immobilisation of microorganisms, especially  
543 *Methanosarcina* and *Methanobacteriums* [142].

544

545 Zeolite has been widely applied to aerobic and anaerobic membrane bioreactor for membrane  
546 fouling reduction. This is because it can improve the settlement of sludge as well as the removal  
547 of nitrogen and phosphorous. As zeolite has high porosity and large surface area, it provides a  
548 stable environment for bacterial attachment, and substantial microbial aggregation can enhance  
549 the settleability of sludge [143]. As a result, membrane fouling can be alleviated by forming  
550 rigid sludge flocs and enhancing membrane permeability. Likewise, the application of zeolite  
551 as a carrier showed effective removal of COD and suspended solid (SS) which could facilitate  
552 better membrane performance and less fouling in anaerobic fluidized membrane bioreactor  
553 [144, 145]. When an anaerobic fluidized membrane bioreactor was operated with natural  
554 zeolites as carriers, the removal rate of SS significantly improved by 22%. It was also observed  
555 that the anaerobic microorganisms were able to attach on the surface of zeolites with  
556 remarkable growth. Thus, no membrane fouling was observed due to the low COD and SS  
557 concentrations [144].

558

### 559 **2.2.7 Beads**

560 The use of granular media fluidizing in AnMBR has been gaining attention along with the  
561 development of anaerobic fluidized bed membrane bioreactor. Previous studies showed that  
562 fluidization of glass beads and polyethylene terephthalate (PET) beads can act as turbulence  
563 promoters and scouring media, respectively, which effectively controlled membrane fouling.  
564 Polymer-based gel beads have also been proved to be an ideal microbial carrier, based on their

565 cost effectiveness, high bio-compatibility, strong stability for long-term use, as well as porous  
566 structure for microbial attachment and aggregation. Moreover, controlling the size and density  
567 of the beads can be achievable by changing the synthesis conditions [146, 147]. Polyvinyl  
568 alcohol (PVA), which is water soluble polymer, can form gel beads by cross-linking with other  
569 materials like sodium alginate and chitosan [148]. Moreover, when PVA and chitosan form  
570 more stable structure through covalent bonds with metal ions, they can be applied in different  
571 fields as adsorbent materials, antibacterial agents, or biocarriers [149, 150]. A research by  
572 Wang et al. [146] showed the effect of PVA/chitosan gel beads and PVA/chitosan/iron gel  
573 beads on anaerobic sludge. Both gel beads favoured the adhesion and aggregation of  
574 methanogens, mainly *Mathanospirillum*, *Methanosaeta* and *Methanobacterium*.

575

576 According to Düppenbecker et al. [151], the use of fluidized glass beads in AnMBR with  
577 external tubular membrane could be a promising option for alleviating membrane fouling in  
578 AnMBRs. The optimal diameter of 1.5-mm fluidized glass beads reduced the fouling despite  
579 the membrane has been damaged by abrasion. Moreover, the COD removal rate was remained  
580 between 77% and 83%, and methane production increased by around 30% as well. The same  
581 research group also evaluated the fouling behaviour by three different ceramic membranes  
582 including ZrO<sub>2</sub> and Al<sub>2</sub>O<sub>3</sub> ultrafiltration membranes and TiO<sub>2</sub> microfiltration membrane. The  
583 presence of fluidized glass beads was able to reduce the fouling rate by around 95% for all  
584 three membranes. Although all types of membranes were damaged by abrasion of glass beads,  
585 Al<sub>2</sub>O<sub>3</sub> microfiltration membrane showed the least abrasion in a clean water filtration test [152].  
586 Similarly, the fluidization of PET beads with bigger size and lower density also demonstrated  
587 significant fouling reduction by scouring the membrane [153, 154]. These fluidized beads can  
588 mitigate membrane fouling by two mechanisms. Firstly, the mixing action of particles can lead



589 to increase in turbulence and thus concentration polarization can be decreased. Secondly,  
590 scouring effect on the previously deposited foulants can also alleviate fouling [151].

591

592 Table 3 lists the effects of the above-mentioned enhancers on AnMBR performance and Table  
593 4 summarizes the advantages and disadvantages of different enhancers for fouling reduction.

on AnMBR performance

Concentration	Configuration of reactor <sup>a</sup>	Feed water	Operating conditions	Effects of other enhancers on performance	References
0.01 g/L	External AnMBR	Bamboo industry wastewater	<ul style="list-style-type: none"> <li>• SRT : 150 d</li> <li>• HRT : 3 d</li> <li>• OLR : 6 kgCOD/m<sup>3</sup>.d</li> <li>• Temperature : 32 ± 2 °C</li> </ul>	<ul style="list-style-type: none"> <li>• Increase in COD removal efficiency by 5%</li> <li>• Increase in biogas production and methane yield</li> <li>• Declined SMP concentration and cake layer resistance</li> <li>• Increased microbial diversity and activity of methanogens</li> </ul>	[86]
0.01 g/L	Biochar-amended external AnMBR	Pharmaceutical wastewater	<ul style="list-style-type: none"> <li>• SRT : 120 d</li> <li>• HRT : 24 h</li> <li>• VSS : 14.67 g/L</li> <li>• OLR : 7 kgCOD/m<sup>3</sup>.d</li> <li>• Temperature : 32 ± 2 °C</li> </ul>	<ul style="list-style-type: none"> <li>• Effective removal of adsorbable organic halogen (AOX) (average 61.5% vs 56.2% without biochar)</li> <li>• Decrease in TMP rising rate by 56%</li> <li>• Slower TMP jump</li> <li>• Reduced proteins of EPS</li> <li>• Decrease in abundance of biofoulant, mainly <i>Arcobacter</i></li> </ul>	[87]
0.01 g/L CWW to W of :50	Submerged AnMBR	Low-grade coal wastewater	<ul style="list-style-type: none"> <li>• HRT : 1 d</li> <li>• COD : 2 g/L</li> <li>• OLR : 1 kgCOD/m<sup>3</sup>.d</li> <li>• Temperature :</li> </ul>	<ul style="list-style-type: none"> <li>• High COD removal efficiency (58%) and methane production (182 CH<sub>4</sub> mL/g COD);</li> <li>• Improved degradation of</li> </ul>	[98]

Iron	N/A	26 mg/L of FeCl <sub>3</sub>	Pilot scale AnMBR	Municipal wastewater	<ul style="list-style-type: none"> <li>• HRT : 8.5 h</li> <li>• SRT : 70 d</li> <li>• Flux : 17 LMH</li> <li>• COD : 383 ± 113 mg/L</li> <li>• pH : 6.7 – 6.8</li> <li>• Temperature : 23 ± 1°C</li> </ul>	<ul style="list-style-type: none"> <li>• Improved COD and BOD<sub>5</sub> removals by 13.8% and 10.8%, respectively</li> <li>• Increased filterability of mixed liquor with reduced colloidal matter</li> <li>• Increased porosity of fouling layer</li> </ul>	[111]
	N/A	150 mg/L of FeCl <sub>3</sub>	AnMBR	Synthetic sewage	<ul style="list-style-type: none"> <li>• Flux : 15 LMH</li> <li>• Feed COD : 500 mg/L</li> <li>• VSS : 5.0-5.5 g/L</li> <li>• Temperature : 35°C</li> <li>• pH : 6 - 7</li> </ul>	<ul style="list-style-type: none"> <li>• Increased sludge floc size and colloids particle size</li> <li>• Reduced thickness of fouling layer</li> <li>• Decreased levels of COD and proteins</li> </ul>	[26]
	Two pairs of electrodes with flat ZVI anodes (90 cm × 5 cm × 0.3 cm) and titanium cathodes (90 cm × 5 cm)		AnMBR	Municipal wastewater	<ul style="list-style-type: none"> <li>• HRT : 10 h</li> <li>• Flux : 15 LMH</li> <li>• Temperature : 35 °C</li> <li>• COD : 483 ± 16 mg/L</li> </ul>	<ul style="list-style-type: none"> <li>• Enhanced COD removal by 3%, and TP removal by 50%, and H<sub>2</sub>S removal (&gt; 500 ppm with electric field vs &lt; 60 ppm without electric field)</li> <li>• Membrane fouling mitigation by the improvement of mixed liquor filterability</li> </ul>	[101]
Calcium	367.5 mg/L of CaCl <sub>2</sub>	100 mg/L	Dead-end microfiltration	Granular sludge mixed liquors from SBR	<ul style="list-style-type: none"> <li>• HRT : 4 h</li> <li>• SRT : 96 d</li> <li>• SS : 5000 mg/L</li> <li>• TMP : 5 kPa</li> </ul>	<ul style="list-style-type: none"> <li>• Reduction of fine particles, colloids and SMP</li> <li>• Limited deposition of fine - particles and colloids on the membrane as cake layer served as a prefilter</li> </ul>	[122]

	2.5 mM of CaCl <sub>2</sub>	100 mg/L	Membrane-coupled EGSB	Synthetic wastewater	<ul style="list-style-type: none"> <li>• HRT : 4 h</li> <li>• COD : 310 – 360 mg/L</li> <li>• pH : 7.0 – 7.5</li> <li>• TMP : 30 kPa</li> <li>• Flow rate : 0.75 L/h</li> </ul>	<ul style="list-style-type: none"> <li>• Decrease in SMP concentration in the effluent by 47.7 - 60.7%</li> <li>• Decline in cake layer resistance by 42.8%</li> <li>• Delayed transition from pore blocking to cake filtration</li> </ul>	[121]
	N/A	500 mg/L	AnMBR	Anaerobic sludge	<ul style="list-style-type: none"> <li>• HRT : 3.4 d</li> <li>• SRT : 40 d</li> <li>• TS : 30.16 g/L</li> <li>• VS : 1.2 g/L</li> <li>• Temperature : 35 °C</li> </ul>	<ul style="list-style-type: none"> <li>• Improved filterability of mixed sludge liquor</li> <li>• Decreased concentration of SMP and zeta potential of sludge</li> <li>• Reduced TMP increase rate</li> </ul>	[130]
Polyaluminum chloride	N/A	200 mg/L	AnCMBR	Phenol- and quinoline-containing wastewater	<ul style="list-style-type: none"> <li>• HRT : 48 h</li> <li>• Flux : 4.32 LMH</li> <li>• MLSS : 35.77 g/L</li> <li>• MLVSS : 20 g/L</li> <li>• Temperature : 35 ± 1°C</li> </ul>	<ul style="list-style-type: none"> <li>• Changes in the structure of bulk sludge and cake layer</li> <li>• Changes in the component of SMP and EPS</li> <li>• Reduced specific resistance to sludge filtration</li> </ul>	[129]
	N/A	500 mg/L	AnMBR	Excess anaerobic sludge	<ul style="list-style-type: none"> <li>• HRT : 3.4 d</li> <li>• SRT : 40 d</li> <li>• TS : 30.16 g/L</li> <li>• VS : 13.22 g/L</li> <li>• Temperature : 35 °C</li> </ul>	<ul style="list-style-type: none"> <li>• Enrichment of anaerobic microorganisms such as <i>Cloacimonetes</i> and <i>Smithella</i></li> <li>• Slightly reduced ratio of VS/TS</li> </ul>	[132]
Zeolite	Natural zeolite (0.2 – 1 nm of pore size, 3 of hardness, 2.1 g/cm <sup>3</sup> of density)	350 mL	AnFMBR	Campus domestic wastewater	<ul style="list-style-type: none"> <li>• HRT : 2.5 h</li> <li>• COD : 130 ± 38 mg/L</li> <li>• pH : 7.2 ± 0.2</li> <li>• Flux : 10 LMH</li> </ul>	<ul style="list-style-type: none"> <li>• Increase in SS removal rate by 22 %</li> <li>• TMP &lt; 0.2 bar</li> <li>• Significant growth of anaerobic microbes on the surface of zeolite</li> </ul>	[144]

					<ul style="list-style-type: none"> <li>• Temperature : 20 - 35 °C</li> </ul>		
Beads	Glass beads (soda-lime glass, 2500 kg/m <sup>3</sup> of density, Worf Glaskugeln, Germany)	4 mm support layer	as AnFMBR	Municipal wastewater	<ul style="list-style-type: none"> <li>• HRT : 1.7 h</li> <li>• SRT : 46 d</li> <li>• COD : 369 ± 98 mg/L</li> <li>• pH : 7.0 – 7.5</li> <li>• TMP : 30 kPa</li> <li>• Temperature : 20 °C</li> <li>• Upflow velocity : 24 – 37 m/h</li> </ul>	<ul style="list-style-type: none"> <li>• Increase in methane production by around 30%</li> <li>• Reduction of the fouling rate by around 95%</li> <li>• Least abrasion by Al<sub>2</sub>O<sub>3</sub> microfiltration membrane</li> </ul>	[151, 152]
	Polyethylene terephthalate beads (3 mm of size and 1.3 of specific gravity)	0.4 v/v packing ratio	of AnFMBR	Synthetic wastewater	<ul style="list-style-type: none"> <li>• HRT : 3.75 h</li> <li>• SRT : 37.5 d</li> <li>• COD : 250 mg/L</li> <li>• pH : 7.0 – 7.5</li> <li>• Temperature : 25 °C</li> <li>• Flux : 10 LMH</li> </ul>	<ul style="list-style-type: none"> <li>• Higher effectiveness when applying PET beads with bigger size and lower density</li> <li>• Significant fouling mitigation by souring</li> </ul>	[153]

595 <sup>a</sup>AnCMBR, anaerobic ceramic membrane bioreactor; AnFMBR, anaerobic fluidized membrane bioreactor; AnMBR, anaerobic membrane bioreactor; EGSB, expanded  
596 granular sludge bed;

597 **Table 2.** Advantages and disadvantages of fouling reduction enhancers

<b>Enhancers</b>	<b>Advantages</b>	<b>Disadvantages</b>
<b>PAC</b>	<ul style="list-style-type: none"> <li>• High adsorption capacity</li> <li>• Increase removal efficiency of COD, fine colloids, colour, and antibiotics</li> <li>• Improve aggregation ability leading to stable sludge flocs</li> <li>• Large surface area than GAC</li> </ul>	<ul style="list-style-type: none"> <li>• Decrease sludge particle size leading to long-term operation</li> <li>• Overdosing can increase membrane fouling due to PAC being a potential fouling agent</li> </ul>
<b>GAC</b>	<ul style="list-style-type: none"> <li>• Improve methane production</li> <li>• Enhance COD, SMP and pharmaceuticals removal</li> <li>• GAC fluidization has lower energy requirement than gas sparging</li> <li>• Scouring effect</li> <li>• Recover can be done by thermal process after adsorption capacity exhausted</li> </ul>	<ul style="list-style-type: none"> <li>• The abrasion can aggravate membrane fouling</li> <li>• Large particles require more energy for fluidization</li> </ul>
<b>Biochar</b>	<ul style="list-style-type: none"> <li>• Improve hydrogen and methane production by enrichment of microorganisms</li> <li>• Decrease SMP and proteins of EPS</li> <li>• Enhance COD removal efficiency and sludge granulation</li> </ul>	<ul style="list-style-type: none"> <li>• Less efficient specific surface area than AC due to non-activated carbon</li> </ul>
<b>Waste yeast</b>	<ul style="list-style-type: none"> <li>• High degradation capacity of phenolic and toxic compounds</li> <li>• Low tendency to adhere on membrane surface</li> <li>• Enhance biogas production</li> </ul>	<ul style="list-style-type: none"> <li>• No significant change in membrane fouling accumulation</li> <li>• Increase SMP and aromatic compounds in permeate group with high molecular weight</li> </ul>
<b>Iron</b>	<ul style="list-style-type: none"> <li>• Enhance sludge granulation and stabilization</li> <li>• Improve methane production and COD removal</li> <li>• Eliminate H<sub>2</sub>S gas</li> <li>• Enhance mixed liquor filterability</li> <li>• Advantageous for long-term operation due to the formation of a precipitate</li> </ul>	<ul style="list-style-type: none"> <li>• Formation of thick cake layer</li> <li>• Cause more severe membrane fouling due to the high concentration of Fe-rich fouling layer</li> </ul>
<b>Calcium</b>	<ul style="list-style-type: none"> <li>• Enhance bioflocculation</li> <li>• Improve accumulation of biomass and degradation of butyrate and acetate acid</li> <li>• Reduce fine particles, SMP,</li> </ul>	<ul style="list-style-type: none"> <li>• Overdosing can lead to membrane precipitation, declined methanogenic activity and inorganic fouling</li> </ul>

	EPS and colloids	
<b>Polyaluminum chloride</b>	<ul style="list-style-type: none"> <li>• High charge neutralization capacity can lead to enlarged floc size and high filtration performance</li> <li>• Improve the abundance of anaerobic microorganisms and hydrogen yield</li> <li>• Reduce the composition rate of carbohydrate in SMP and EPS</li> <li>• The cake layer become more porous and looser</li> </ul>	<ul style="list-style-type: none"> <li>• High concentration can inhibit SCFAs production and decrease phosphorous</li> </ul>
<b>Zeolite</b>	<ul style="list-style-type: none"> <li>• High ion exchange capacity can enhance ammonia and heavy metals removal</li> <li>• Improve methane production, COD, nitrogen and phosphorous removal</li> <li>• Enhance sludge settlement by bacterial attachment and aggregation</li> </ul>	
<b>Beads</b>	<ul style="list-style-type: none"> <li>• Fluidization of PET beads can act as turbulence promoters and scouring media</li> <li>• Polymer-based gel beads have cost effectiveness, high bio-compatibility, high stability for long-term use, and porous structure for microbial attachment and aggregation</li> <li>• The size and density can be controlled by different synthesis conditions</li> <li>• Increase COD removal rate and methane production</li> </ul>	<ul style="list-style-type: none"> <li>• Fluidization of glass beads can damage membrane by abrasion</li> </ul>

599 **3. Future perspectives**

600 Membrane fouling is one of the most challenging issues in operating MBR processes.  
601 Pretreatment of feed wastewater can effectively mitigate membrane fouling by changing the  
602 feed properties. The addition of fouling reduction enhancers to bioreactors as adsorbents,  
603 coagulants/flocculants and suspended carriers can significantly modify the feed characteristics.  
604 To date, there have been investigations of many different enhancers applied to aerobic MBRs  
605 for the purpose of fouling control and improvement of bioreactor performance. However, only  
606 a limited number of studies were available to investigate the effects of enhancers' addition in  
607 AnMBRs and only a few types of enhancers were studied previously. Hence, it is necessary  
608 and important not only to study the application of novel enhancers in anaerobic treatment, but  
609 also to understand the fouling reduction mechanisms of each enhancer under anaerobic  
610 condition.

611

612 As discussed in this review, previous studies have applied several enhancers to AnMBRs. The  
613 addition of activated carbon, such as PAC and GAC, has proven to be effective solution to  
614 alleviate membrane fouling. Both PAC and GAC could act as a supporting medium for the  
615 growth of anaerobic microorganisms due to its high adsorption capacity. PAC could effectively  
616 adsorb colloids and dissolved organic matters in AnMBRs, while GAC mainly adopted as  
617 fluidized media and could scour membrane as well as enhance methane production.  
618 Throughout the organic and inorganic enhancers, biochar and zeolite could be applied as  
619 adsorbents, while calcium was able to act as flocculants. In addition, iron and PACl were added  
620 as coagulants, and waste yeast and beads could perform as co-substrates and biocarriers,  
621 respectively.

622



623 However, overdosing or large particle size of enhancers caused more severe membrane fouling  
624 and deterioration of removal performances, due to their potential to become a foulant. Although  
625 optimal PAC replenishment ratio for effective fouling mitigation in aerobic MBR was reported  
626 to be 1.67%, the refreshment ratio of PAC or GAC in AnMBR remains as a challenging issue  
627 [155]. Thus, further studies regarding the optimization of the dosage as well as replacement  
628 ratio of enhancers should be carried out for the best improvement of performance as well as  
629 controlling membrane fouling. Furthermore, more studies on the different types of novel  
630 enhancers, such as waste yeast and beads, are necessary, because there are much less number  
631 of studies compared to that of activated carbon. Additionally, more research regarding the long-  
632 term effect of enhancers is also required, since they may influence negatively on AnMBR  
633 performance during long-term operation. Moreover, it is also important to consider the lifespan  
634 of membrane itself, when enhancer is added. The addition of particulate enhancers, such as  
635 PAC, GAC and biochar, could greatly mitigate irreversible membrane fouling and prolong the  
636 lifespan of membrane. However, comparatively large particle size or fluidization of GAC and  
637 glass beads could lead to abrasion and damage on membrane. Therefore, more research on the  
638 membrane lifespan with enhancers is also required for better understanding on the performance  
639 of enhancers.

640

641 In spite of many applications and research have been carried out in AnMBR with various  
642 enhancers, most of the research is confined to lab scale experiments. The major obstacle  
643 limiting scale up and wider application of AnMBRs can be membrane fouling, as membrane is  
644 one of the main contributors to capital and operational costs in AnMBRs. The capital cost of a  
645 full-scale submerged AnMBR system was about 800 USD/m<sup>3</sup>/day. It was also estimated that  
646 almost 72.3% of capital cost accounted for membrane fraction with the assumed capacity of  
647 20000 m<sup>3</sup>/day, which was higher than that of aerobic MBR system (25-60%) [1, 156]. On the

648 other hand, the operational cost including gas scouring, pumping and sludge disposal for  
649 submerged AnMBR was reported to be almost one third of that of aerobic MBR system, which  
650 was about USD 235000/year and USD 822741/year, respectively [156]. Thus, the full-scale  
651 AnMBR system could be economically feasible by adopting solutions such as low cost filters.

652

653 Since the energy requirement for membrane fouling control in AnMBR accounted more than  
654 75% of the total energy requirement, it is important to apply efficient fouling control strategies  
655 in terms of energy consumption and costs. As discussed in section 2.1.2, GAC fluidization had  
656 lower energy consumption than gas sparging. The addition of enhancers such as  $\text{FeCl}_3$  required  
657 much lower energy of  $0.08 \text{ kWh/m}^3$  due to the lack of rotation [157]. In terms of cost, activated  
658 carbon (0.6-20 USD/kg) and biochar (0.2-0.5 USD/kg) could be relatively cheaper compared  
659 to other chemical enhancers [158]. Therefore, careful consideration and further analysis of  
660 enhancers for practical AnMBR application should be conducted.

661

662 To sum up, further studies on the optimisation of the adequate dosage and the impact of  
663 different particle size of each enhancer should be done in the near future, accompanied by the  
664 investigation of long-term impact. Moreover, the interaction mechanisms between the  
665 enhancers and anaerobic microbial activities also needs further exploration to better understand  
666 the influences on membrane fouling mitigation. Since the scale-up from bench-scale  
667 experiment to full-scale application is not simple, it is necessary to research further for the wide  
668 implementation of full-scale AnMBR with minimized membrane fouling.

669

670 **3. Conclusion**

671 The main conclusions in this review are as follows:

- 672 • The addition of fouling reduction enhancers, including activated carbon, biochar, zeolite,  
673 and polyaluminum chloride, could effectively alleviate membrane fouling in AnMBRs.
- 674 • Enlarged floc size and decreased soluble organics mainly contributed to the mitigation of  
675 fouling.
- 676 • Overdosing or large particle size of enhancers could lead to contrary result due to their  
677 potential to be a foulant.

678

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684

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