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1 **Simultaneous nutrient recovery and algal biomass production from anaerobically**
2 **digested sludge centrate using a membrane photobioreactor**

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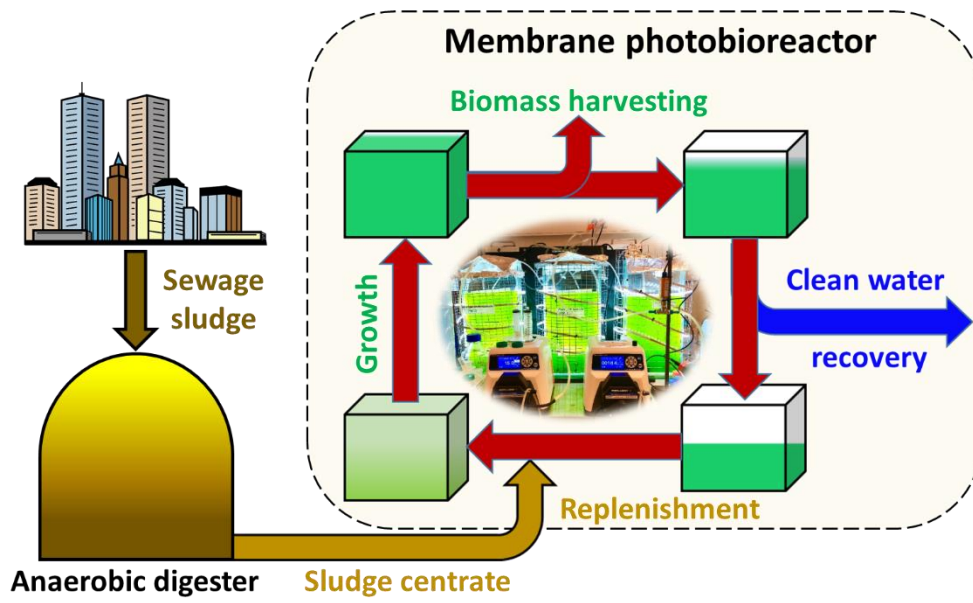
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32 **Graphical abstract**



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34

35 **Highlight**

- 36 • Continuous algae growth could be achieved by MPR using sludge centrate.
- 37 • Nutrient loading had indiscernible impact on biomass growth.
- 38 • Nutrient removal efficiency increased as nutrient loading rate decreased.
- 39 • Nutrient removal efficiency increased as HRT increased.
- 40 • Backwashing completely restored water flux decline caused by microalgae deposition.

41

42 **Abstract**

43 This study aims to evaluate the performance of *C. vulgaris* microalgae to simultaneously
44 recover nutrients from sludge centrate and produce biomass in a membrane photobioreactor
45 (MPR). Microalgae growth and nutrient removal were evaluated at two different nutrient
46 loading rates (sludge centrate). The results show that *C. vulgaris* microalgae could thrive in
47 sludge centrate. Nutrient loading has an indiscernible impact on biomass growth and a notable
48 impact on nutrient removal efficiency. Nutrient removal increased as the nutrient loading rate
49 decreased and hydraulic retention time increased. There was no membrane fouling observed in
50 the MPR and the membrane water flux was fully restored by backwashing using only water.
51 However, the membrane permeability varies with the hydraulic retention time (HRT) and
52 biomass concentration in the reactor. Longer HRT offers higher permeability. Therefore, it is
53 recommended to operate the MPR system in lower HRT to improve the membrane resistance
54 and energy consumption.

55 **Keywords:** Biomass production; *C. vulgaris*; membrane photobioreactor; nutrient recovery;
56 sludge centrate.

57 **1. Introduction**

58 Municipal wastewater is a valuable resource in a circular economy because it can be used
59 to recover and reuse energy, nutrients, and clean water (Ansari et al., 2016; Nguyen et al.,
60 2021; Vu et al., 2021b). In wastewater treatment plants (WWTPs), most of the organic input
61 from wastewater is anaerobically digested to produce biogas which is a source of clean
62 energy and digestate (a mixture of solid and liquid residue from anaerobic digestion) (Vutai
63 et al., 2016). Digested sludge centrate is the liquid fraction after digestate dewatering that
64 has been reported as the concentrated source of nutrients (i.e. nitrogen and phosphorus).
65 The ammonia and phosphate contents in sludge centrate can reach up to 1 and 0.5 g/L,
66 respectively (Li et al., 2020; Liu et al., 2021; Vu et al., 2021b; Wang and Lee, 2021). The
67 high nitrogen and phosphorus content in a small volume of sludge centrate offers an excellent
68 opportunity for nutrient recovery.

69 Nutrient recovery from sludge centrate is a win-win solution for nutrient management in
70 WWTPs. Even if only 30% of nutrients in sewage end up in sludge centrate, the standard
71 practice of returning this stream to the headwork for further treatment can have a negative
72 impact on WWTPs (Abey Siriwardana-Arachchige et al., 2020). Examples include nutrient
73 organic carbon imbalance, struvite blockage, and failure to meet stringent effluent discharge
74 standards (Ansari et al., 2016; Vu et al., 2019). Thus, nutrient recovery from sludge centrate
75 can simultaneously improve compliance with effluent discharge standards while also
76 lowering maintenance costs due to the significant reduction in struvite blockage. At the same
77 time, valuable fertilizers can be made from the recovered nutrients.

78 To date, several techniques have been developed and applied to recover nutrients from
79 wastewater, such as sludge centrate. Examples include direct stripping (Ye et al., 2020), ion
80 exchange (Wirthensohn et al., 2009), electrodialysis (Ward et al., 2018), chemical
81 precipitation (Ansari et al., 2016; Daneshgar et al., 2018), membrane filtration (Ansari et al.,
82 2016; Shin et al., 2021), and microbial electrochemical processes (Barua et al., 2019;
83 Nancharaiah et al., 2016). They have proven their efficacy and potential in recovering
84 nutrients from wastewater. However, majority of these processes are primarily focused on
85 phosphorus recovery rather than a combination of both nitrogen or phosphorus (Barua et al.,
86 2019). Furthermore, high chemical and energy consumptions continue to be major barriers to
87 commercialisation of these technologies (Ansari et al., 2016; Cong Nguyen et al., 2020;
88 Ward et al., 2018)

89 Microalgae-based treatment has recently emerged as a cost-effective and environmentally-
90 friendly method of removing and recovering nutrients from wastewater (Abeywardana-
91 Arachchige et al., 2020; Ahmed et al., 2022). Microalgae use sun light as the energy source,
92 carbon dioxide from the atmosphere as the carbon source, and nitrogen and phosphorus from
93 wastewater to grow. Microalgae based wastewater treatment has numerous advantages
94 including low operating costs (Ahmed et al., 2022), carbon capture (Deprá et al., 2020;
95 Nagarajan et al., 2019), the production of biochemical feedstock (Khoo et al., 2019), and
96 biofuel from algal biomass (Vo et al., 2018).

97 Microalgae-based treatments for removing nutrients from wastewater and producing
98 biomass in photobioreactors have been demonstrated in several studies (Sayed et al., 2020;
99 Zhou et al., 2017). Zhou et al. (2017) reported that *Spirulina platensis* in saline wastewater
100 could remove 80% of total nitrogen and 93% of total phosphorus, and achieve 0.76 g/L in
101 biomass content. In a more recent study, Sayed et al. (2020) showed nitrogen and
102 phosphorus removal efficiencies of 95% and 78% from anaerobic digestate, respectively, by
103 *Chlorella sorokiniana*. However, microalgae-based technology has a high space requirement,
104 thus, it has been rarely commercially applied for removing nutrients from wastewater (Gao et
105 al., 2016). A major technical challenge is to increase the microalgae content in the reactor for
106 process intensification and reduction in space requirement (Gao et al., 2016; Nguyen et al.,
107 2020).

108 The aforementioned challenge can be addressed by incorporating a submerged
109 ultrafiltration membrane with the bioreactor to form a membrane photobioreactor (MPR). In
110 the MPR, a high algal biomass concentration can be achieved at a low hydraulic retention
111 time allowing for process intensification. Furthermore, this method can be easily scaled up.

112 Therefore, this study aims to evaluate the effectiveness of an MPR following an ingenious
113 operation cycle in simultaneously recovering nutrients and producing microalgal biomass
114 from sludge centrate. The feasibility of continuous operation of the microalgae system is
115 demonstrated via monitoring its stable performance. Additionally, the effects of hydraulic
116 retention duration and the rate of sludge centrate loading on nutrient removal and biomass
117 generation are investigated. The results from this study are expected to be a stepping-stone to
118 valorise resources from high strength wastewater.

119

120 **2. Materials and methods**

121 **2.1. Microalgae inoculum and sludge centrate**

122 The freshwater green microalgae strain *C. vulgaris* (CS-41) from the Australian National
123 Algae Culture Collection, CSIRO Microalgae Research (Hobart, TAS, Australia) was used in
124 this study. The microalgae were incubated in MLA medium at the University of Technology
125 Sydney culture collection (Vu et al., 2021a). A concentrated microalgae solution was
126 prepared from the culture collection and used as inoculum. This was accomplished by
127 removing the supernatant from the culture and centrifuging the remainder at 3,000 rpm for 5
128 minutes.

129 Sludge centrate from a high speed centrifuge at a full scale wastewater treatment plant
130 (located in Sydney, Australia) was used as the nutrient source to cultivate the microalgae.
131 Large particles were removed from the sludge centrate using a 75 μm stainless steel filter
132 mesh. The raw sludge centrate is at pH 6.95 and had 253 mg/L COD, 998 mg/L $\text{NH}_3\text{-N}$, and
133 312 mg/L PO_4^{3-} . The total nitrogen (TN) and total phosphorus (TP) were 1012 and 318 mg/L,
134 respectively.

135 **2.2. Experimental systems**

136 Three identical 3.5 L glass reactors were used to cultivate microalgae (Supplementary
137 Data). The internal dimensions of each reactor were 20 cm in length, 4 cm in width, and 45
138 cm in height. In order to ensure adequate mixing, each reactor's microalgae culture was
139 aerated at a rate of 1 L/min using a stone diffuser positioned at the bottom of the reactor. The
140 air was cleaned using a 0.45 μm cartridge filter. The reactor was illuminated with a
141 surrounding LED strip at a light intensity of approximately 100 $\mu\text{mol}/\text{m}^2/\text{s}$ in a 16:8 -hour
142 light:dark cycle. This light/dark cycle condition has been established in our previous work as
143 a favourable condition for *C. vulgaris* growth (Nguyen et al., 2020). These operational
144 conditions were consistent throughout the experiments regardless of the operation modes of
145 the microalgae reactor.

146 In the MPR, a polyvinylidene difluoride ultrafiltration (UF) hollow fiber membrane
147 module (Mitsubishi Rayon Co., Ltd) was used to withdraw the treated water (Figure 1A). The
148 nominal pore size and total surface area of the module were of 0.04 μm and 0.073 m^2 ,
149 respectively. A Masterflex Peristaltic pump (Cole-Parmer, USA) connected to the membrane
150 module was used to extract clean water from the MPR. A pressure transducer (PT30 model,
151 Extech Instruments, United States) was inserted in the suction line of the pump to monitor the
152 changes in transmembrane pressure during operation.

153 **2.3. Experimental protocols**

154 Microalgae growth and nutrient removal were evaluated at two nutrient (sludge centrate)
155 loading rates. The feed solutions to the MPR were prepared by diluting raw sludge centrate
156 12.5 and 25 times using clean water corresponding to high and low nutrient loading rates,
157 respectively. This work aims to demonstrate the effectiveness of the MPR in maintaining
158 stable performance in terms of microalgae growth and nutrient removal. Therefore, the
159 pretreated sludge centrate (section 2.1) was further filtered through 1 μm filter paper prior to
160 the dilution step in order to minimise any impacts caused by the presence of bacteria and
161 turbidity in the medium.

162 Microalgae cultures in three reactors were inoculated simultaneously using diluted sludge
163 centrate corresponding to each nutrient loading rate presented earlier. Each reactor were
164 inoculated by dosing 50 mL of the concentrated microalgae culture (section 2.1) into 2950
165 mL of diluted sludge centrate in order to achieve a biomass content of approximately 145
166 mg/L. Each reactor had a working volume of 3 L. During the stationary phase, one reactor
167 remained in batch mode. The other two reactors were switched to the MPRs at HRT of 3 and
168 5 days, respectively.

169 Algal biomass extraction and sludge centrate feeding were conducted once a day in four
170 steps (Figure 1B). First, 100 mL of the microalgae culture was collected from each reactor,
171 which was subsequently used for the measurement of biomass content and nutrient removal.
172 Second, 900 and 500 mL of treated water were extracted through the membrane from each
173 reactor over 1 hour corresponding to HRT of 3 and 5 days, respectively. In practice, the
174 treated water from a microalgae system would be mixed with the raw feed solution for the
175 next cultivation cycle. In this study, the treated water was not reused for cultivation so that a
176 constant nutrient loading can be achieved for systematic comparison. Instead, the above
177 described fresh culture media were used for daily feeding the system. Third, after the
178 filtration process, fresh diluted sludge centrate solution was fed to the reactor to maintain the
179 HRT of 3 and 5 days, respectively. Finally, the microalgae reactor was operated under steady
180 conditions for the remaining duration of the day.

181 **[FIGURE 1]**

182 At the end of the MPR experiment, membrane permeability was measured at the final
183 microalgae content in the reactor. The initial membrane flux was adjusted to 20 L/m².h and
184 the transmembrane pressure during filtration was recorded for 150 min for permeability
185 calculation. During the permeability tests, the permeate was returned to the reactor to

186 maintain constant liquid volume and microalgae concentration. The MPR was continuously
187 aerated with air at 1.5 L/min through a diffuser placed in the bottom of the reactor. The
188 permeability test was conducted in replication. At the end of each filtration cycle, the
189 membrane module was backwashed at 40 L/m².h using clean water and aerated at 1.5 L/min
190 for 5 min.

191 **2.4. Analytical methods**

192 Chemical oxygen demand (COD) was measured by the US-EPA Standard Method 5220
193 using a HACH DRB200 COD reactor and HACH DR3900 spectrophotometer. Ammonium
194 (NH₃-N), total nitrogen (TN) and total phosphorus (TP) were determined by HACH standard
195 kits using the HACH DR3900. Orthophosphate (PO₄³⁻) was measured using ion
196 chromatography (IC) (Thermo Fisher, Australia). The system was equipped with a Dionex
197 AS-AP auto-sampler and a Dionex AS19 IC column (7.5 µm pore size, 4 mm diameter and
198 250 mm length). The sample injection volume was 10 µL. The analysis conducted using
199 potassium hydroxide eluent with the following gradient (time [min]: concentration [mM]) (0-
200 10: 10; 10-25: 45; 25-27: 45; 27-30: 10; 31: stop run).

201 The optical density and dry weight of microalgae culture were determined daily using a
202 UV spectrophotometer (UV 6000 Shimadzu; Australia) at a wavelength of 680 nm and by
203 gravimetric analysis, respectively to assess microalgae growth. For the optical density
204 measurement, 3 mL of homogeneous microalgae cell suspension was transferred into a
205 cuvette to measure the optical density. For gravimetric analysis, 50 mL of microalgae cell
206 suspension was filtered through a 1.1 µm pre-weighed glass filter paper. The filter paper was
207 then dried at 60 °C for 4 hours to a constant mass. A linear regression coefficient (R²) of 0.96
208 was confirmed between the optical density and dry weight biomass.

209

210 3. Results and discussions

211 3.1. Biomass production

212 Results in Figure 2A confirm that microalgae can thrive in sludge centrate. At both
213 nutrient loading rates, there was no observable lag phase, which indicates good adaption of *C.*
214 *vulgaris* to sludge centrate as the growth medium (Figure 2A). In batch mode, the microalgae
215 grew rapidly and reached a stationary phase with a biomass concentration of 1,100 mg/L at
216 day 6 at both loading rates. The specific growth rates under both nutrient loadings were
217 similar at 0.34 day⁻¹ in batch mode. The biomass content and specific growth rate in this
218 study were similar or higher than those reported in previous studies using nutrient rich
219 effluent or aquaculture wastewater as culturing media (Boonchai and Seo, 2015; Gao et al.,
220 2016). Results in this study confirm that sludge centrate was sufficient to maintain high
221 microalgal biomass productivity. Another reason is that biomass production could be
222 promoted by the heterotrophic growth of *C. vulgaris* with the presence of organic carbon in
223 sludge centrate (Gim et al., 2016).

224 In batch mode, the microalgae population collapsed after 12-14 days of continuous
225 operation (Figure 2A). This ecological collapse is expected and mainly due to the limited
226 illumination and depletion of limiting nutrients, especially nitrogen, as evidenced by the
227 complete removal of ammonia in the effluent in batch mode at the stationary phase (see
228 supplementary material). In addition, beyond the stationary phase, the microalgae cultures
229 were highly alkaline at pH 9.35 (data not shown), which was unfavourable for *C. vulgaris*
230 growth (Sakarika and Kornaros, 2016). The observed phenomenon is consistent with the
231 growth stages of microalgae (i.e. lag, exponential growth, stationary, and death stages) in
232 previous photobioreactor studies (Vo et al., 2018; Vu et al., 2020).

233 By contrast to batch mode, the MPR could achieve stable biomass production (Figure
234 2B&C). In the MPR, regular extraction of microalgal biomass and treated water as well as the
235 replenishment of fresh feed improved the biomass production at both nutrient loading rates.
236 Biomass content in the MPR was 40% higher than that in batch mode (at HRT of 3 days).
237 The observed improved biomass content in the MPR was due to the retention of microalgal
238 biomass by the membrane. The sufficient supply of nutrients from daily fresh feed
239 replenishment to the MPR could also promote the growth of microalgae, thus increasing
240 biomass content. While the main focus of this study was on microalgae growth in the MPR,

241 additional work is also recommended to examine any long term changes in cell morphology
242 and content caused by sludge centrate.

243 In the MPR, nutrient loading did not show any discernible impact on biomass growth
244 (Figure 2). The microalgal biomass contents at low and high nutrient loading rates were
245 similar in the MPR (Figure 2B and 2C). This is because in the MPR, the system is not limited
246 by nutrients. Microalgal biomass content in the MPR of approximately 1.6 g/L in this study is
247 much higher than that (i.e. approximately 0.9 – 1.1 g/L) reported in previous works in the
248 literature (Gao et al., 2016; Nguyen et al., 2020). Thus, illumination for photosynthesis has
249 probably become the limiting factor in this study. Furthermore, feeding the reactor with high
250 ammonium content (approximately 80 mg/L) on a daily basis may cause toxicity to *C.*
251 *vulgaris* microalgae, reduce cell viability, and retard the biomass production (Collos and
252 Harrison, 2014; Zheng et al., 2019).

253 [FIGURE 2]

254 In MPR mode, microalgal biomass production is regulated by HRT. A low HRT resulted
255 in higher microalgal biomass production (Figure 2B and 2C). The impact of HRT on
256 microalgal biomass production was more profound at the low nutrient loading rate. This is
257 because the larger volume of withdrawal effluent and the replenishment of fresh feed could
258 result in better control of the culture pH and improved illumination for microalgae growth.
259 The obtained pH values of the microalgae culture using the low rate of sludge centrate at
260 HRT of 3 and 5 days after stabilisation of biomass growth were approximately 7.6 and 8.3,
261 respectively.

262 **3.2. Organic matter and nutrient removal from sludge centrate**

263 The removal of COD by *C. vulgaris* microalgae was minimal. This outcome is expected
264 because microalgae are autotrophs, meaning they can obtain energy from light and grow
265 using CO₂ rather than organic carbon to grow. There is an increase in COD residue from
266 sludge centrate addition in the effluent (Figure 3). Nevertheless, the COD residue reached an
267 equilibrium after about four days in the MPR. The observed increase in COD residue is due
268 to the dilution effect at the beginning of the MPR operation and initial chemoautotrophic
269 microalgae growth. In batch mode, COD was removed completely by the microalgae culture,
270 which could be attributed to *C. vulgaris*'s chemoautotrophic growth and enhanced organic
271 carbon metabolism under nitrogen-starved conditions (Su, 2021).

272

273 **[FIGURE 3]**

274 At the beginning of the MPR operation, nutrient content in the treated water remained at a
275 low level as evidenced by the high removal efficiency over the first few days (Figure 4). This
276 initial increase in nutrient removal can also be attributed to the dilution effect discussed
277 above in relation to COD removal. Nutrient removal eventually reached a stable value in all
278 experiments as the equilibrium of nutrient input and output was reached.

279 Nutrient loading rate has a significant impact on nutrient removal efficiency (Figure 4).
280 Nutrient removal at the high loading rate was only half of that at the low loading rate. As
281 discussed in section 3.1, increased nutrient loading did not affect biomass growth. The main
282 mechanism of nutrient removal is mentioned to be biomass production combined with
283 nutrient consumption for microalgae assimilation. Thus, higher nutrient input and low
284 utilisation for biomass growth could result in higher nutrient content in the effluent and
285 decreased removal efficiency.

286 **[FIGURE 4]**

287 HRT also has a significant impact on nutrient removal efficiency (Figure 4). On average,
288 80% ammonia and 72% phosphate could be removed from sludge centrate at low nutrient
289 loading rate with HRT of 5 days. Under low nutrient loading rate, 5 days HRT showed better
290 nutrient removal with approximately 30% increase compared to 3 days HRT. This result
291 could be attributed to more adequate contact time for the nutrient assimilation by microalgae
292 at longer HRT. Furthermore, the elevated pH (i.e. pH 8.3) of the culture after 5 days HRT
293 could promote ammonia volatilisation, thus increasing nitrogen removal efficiency.

294 **3.3. Membrane permeability**

295 Backwashing completely reversed the membrane water flux. This was demonstrated by
296 insignificant differences in the initial membrane permeability between duplicate experiments
297 regardless of HRTs (Figure 5). The change in the membrane permeability followed a similar
298 pattern throughout the specific filtration process. The membrane permeability decreased
299 significantly during the first 60 minutes and then remained stable (Figure 5). The rapid
300 deposition of microalgae cells on the membrane surface caused by high hydrodynamic drag
301 force could explain the significant reduction in permeability during the early stages of
302 filtration. The constant permeability after reaching a steady-state value could be attributed to
303 the equilibrium of deposition phenomenon, which occurred as a large number of microalgae
304 cells were swept away from the membrane surface by the shear force generated by the
305 aeration in the reactor.

[FIGURE 5]

306
307 The permeability of the membrane was determined by the amount of biomass in the
308 reactor (Figure 5). Longer HRT (i.e. 5 days) resulted in higher permeability (Figure 5). The
309 longer HRT with lower biomass concentration, as shown in section 3.1, could reduce the
310 severity of microalgae deposition on the membrane, thus improving the permeability. A
311 higher permeability value indicates that the membrane resistance is low and that a larger
312 volume of the medium can be filtered in the same amount of time. These findings imply that
313 operating the MPR at short HRT is recommended due to the low membrane resistance and
314 consequently lower energy consumption.

315 **4. Conclusion**

316 The feasibility of using an MPR for simultaneous nutrient recovery and algal biomass
317 production from anaerobic sludge centrate was demonstrated. In this study, it can be
318 concluded that in comparison to the batch mode reactor, the MPR allows for continuous
319 cultivation of microalgae with 40% higher biomass content. The effects of nutrient loading on
320 biomass growth were negligible. Reduced nutrient loading rate and increased HRT resulted in
321 improved nutrient removal efficiency. The permeability of the membrane was determined by
322 the amount of biomass in the reactor. After backwashing using only water, the water flux
323 could be fully recovered.

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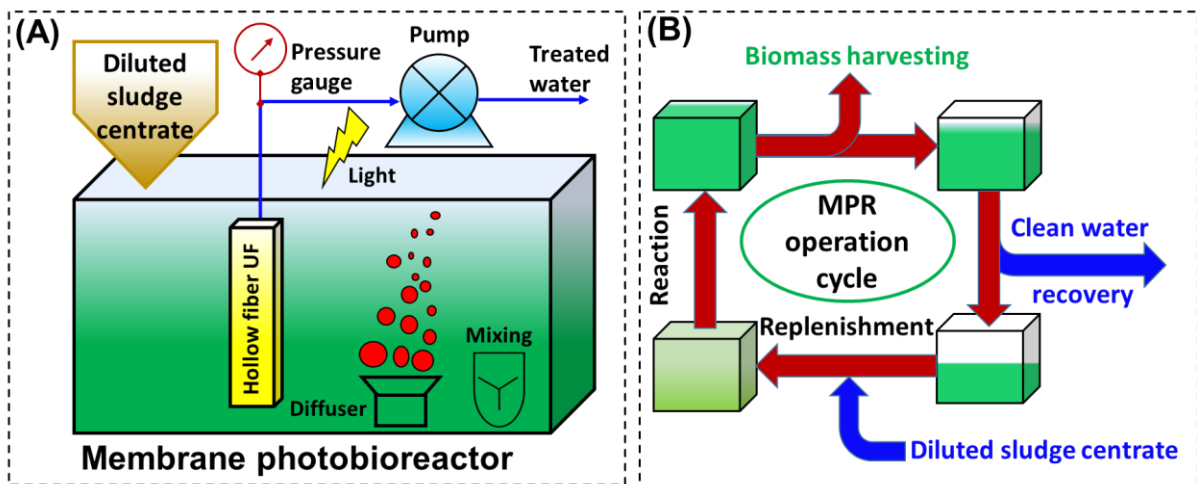
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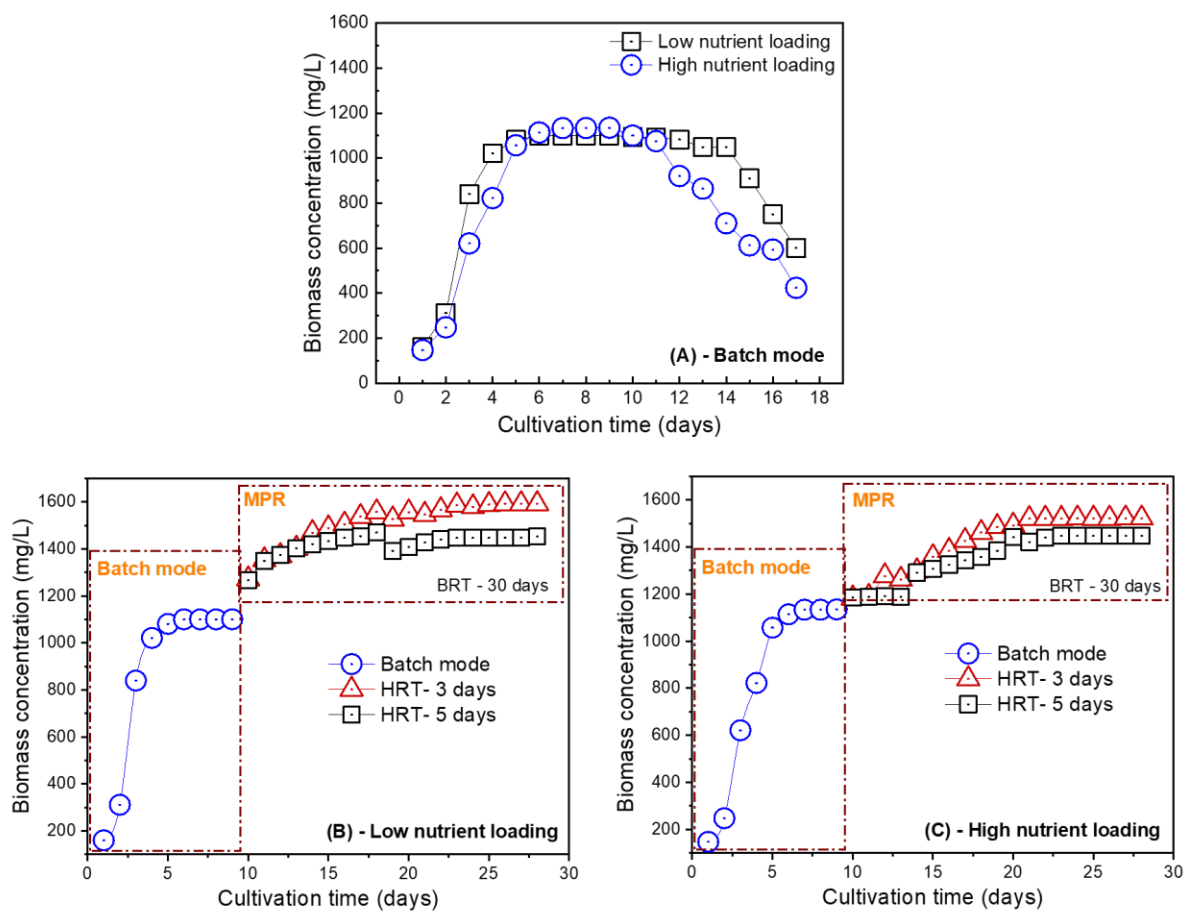
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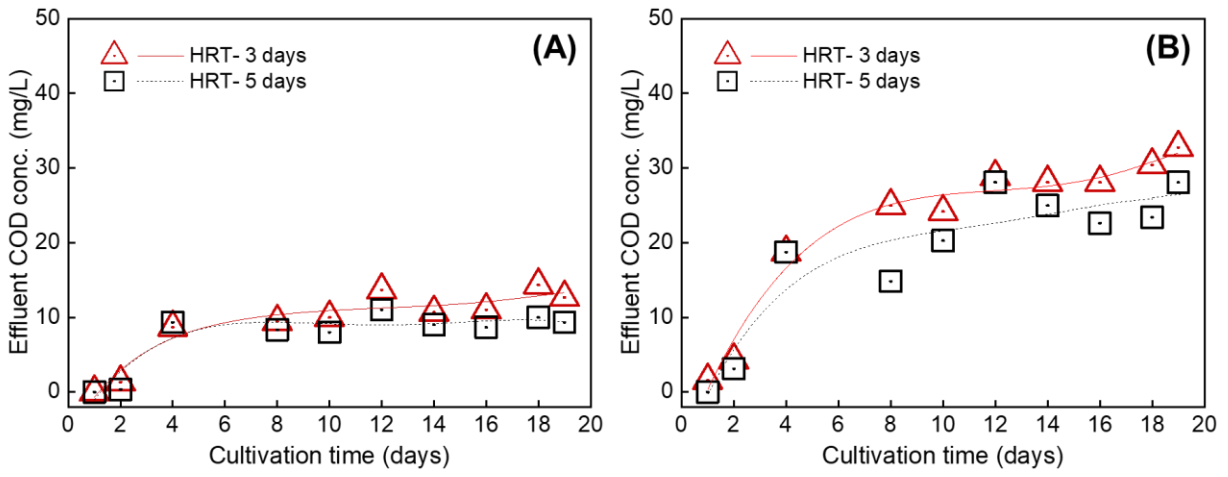
441 **List of Figures**



442
 443 **Figure 1.** Schematic diagram of experimental systems in this study, which presents (A)
 444 membrane photobioreactor and (B) MPR operation cycle.



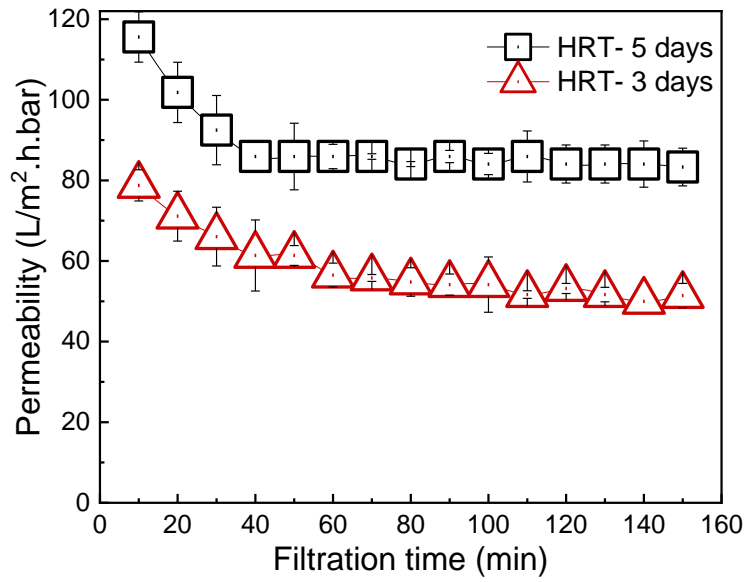
445
 446 **Figure 2.** Changes in biomass production of (A) batch mode microalgae reactor and the MPR
 447 at (B) low nutrient loading and (C) high nutrient loading.



448

449 **Figure 3.** Changes in COD concentration in the MPR effluent (permeate) over time at (A)

450 low and (B) high rate of sludge centrate and different HRTs.



454

455 **Figure 5.** Comparison in membrane permeability of microalgae culture at low loading rate of
 456 sludge centrate and different HRTs. Values and error bars are the mean and standard
 457 deviation of two replicate experiments.

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