### Modelling and Control of Smart Structures Embedded with Magnetorheological Dampers

Minh Tam Nguyen

A thesis submitted in fulfilment of the requirements for the degree of Doctor of Philosophy

Faculty of Engineering and Information Technology University of Technology, Sydney, Australia

December 2009

#### **CERTIFICATE OF AUTHORSHIP/ORIGINALITY**

I certify that the work in this thesis has not previously been submitted for a degree nor has it been submitted as part of requirements for a degree except as fully acknowledged within the text.

I also certify that the thesis has been written by me. Any help that I have received in my research work and the preparation of the thesis itself has been acknowledged. In addition, I certify that all information sources and literature used are indicated in the thesis.

Production Note: Signature removed prior to publication.

Minh Tam Nguyen

#### Abstract

Civil structures are designed with certain stiffness and damping to withstand certain loads. As a result of inadequate damping, earthquakes or strong winds may cause damage or even collapse to civil structures. Structural control devices have therefore been developed and installed in structures to help mitigate such extreme seismic vibrations. There are three types of structural control devices, namely passive, active and semi-active devices according to their energy consumption.

i

The magnetorheological (MR) dampers are considered to be semi-active devices and increasingly employed in structural control applications owing to many feasible advantages. The forces generated by MR dampers can be adjusted by applying an external magnetic field to the MR dampers. They can operate in a passive mode and their power consumption in active mode is very small compared to that of active control devices. However, a major drawback hindering their application exists due to their non-linear force/displacement and hysteretic force/velocity characteristics.

The modelling and control of MR dampers embedded in civil structures to mitigate seismic responses constitute the objective of this research. With regard to structural control, it is crucial that a tractable model of the MR damper is available before any realisable controller can be designed. There are several models for MR dampers in the literature, such as the Bingham, Bouc-Wen, phenomenological models, among others. In refining the modelling of MR dampers to be used in certain aspects of the control design and analysis, this thesis proposes some new models, namely the non-symmetric hysteresis Bouc-Wen model, the static hysteretic model and the polynomial fitting model. The non-symmetric hysteresis Bouc-Wen model is based on the original Bouc-Wen model but takes into account the effect of non-symmetrical hysteresis of the force/velocity relationship. The static hysteretic model makes use of a hyperbolic tangent function to represent the hysteresis, and linear functions to represent the damping and stiffness. The polynomial fitting model is based on the curve fitting approach, whereby the hysteretic behaviour of the MR damper is represented by a mixture of a sigmoid function and a Gaussian function.

There are several control strategies developed in literature such as a well-known clipped-optimal control, Lyapunov-based control, sliding mode control (SMC), and so on. In these strategies the currents supplied to MR dampers are determined indirectly from the desirable MR damper forces obtained from the controllers. In this research, a Lyapunov-based controller and a Linear Quadratic Regulator (LQR) controller that can directly control the currents supplied to MR dampers are developed with the aim of improving the control performance. Furthermore, the dampers are configured in a differential mode to counteract the force-offset problem from the use of a single damper.

The effectiveness of the proposed controllers is verified in both intensive simulations using a multi-storey building model subject to quake-like excitations, and experiment, in part using a physical building model excited by quake-like vibrations from the shaking table at the University of Technology Sydney (UTS).

#### Acknowledgements

First of all, I would like to express my sincerest gratitude and appreciation to my principal supervisor, A/Prof. Quang Ha, for his guidance, patience and support throughout my candidature here at the University of Technology, Sydney (UTS). My special thanks also go to my alternative supervisor, Dr Sarath Kodagoda, for his help and encouragement.

I would like to take this opportunity to thank Dr N.M. Kwok for his valuable advice, assistance and support during my candidature.

Thanks also go to Mr. T.H. Nguyen and Mr. S.M. Hong for their kind support.

I wish to thank Prof. Hung Nguyen, Associate Dean of UTS Faculty of Engineering and Information Technology; Prof. Gamini Dissanayake, Director of the UTS node of CAS; and Prof. Bijan Samali, the group head of the Infrastructure and the Environment engineering group at UTS, for their kindness and support.

Thanks also go to Dr Jianchun Li, Dr Yangchen Li, Mr. Rami Haddad, and Mr. Laurence Stonard for their valuable assistance and feedback in conducting the experiments.

To all my friends here in Australia and my colleagues in the Ho Chi Minh City University of Technical Education, I also thank you for making my life more enjoyable.

Thanks also go to Sue Felix for proofreading my work.

Financial support for this work has come from a number of sources, including the Vietnam Ministry of Education and Training, the Australian Research Council (ARC) and the New South Wales State Government. Without this support, this work could not have been finished.

I thank God for being forgiving, for looking after and protecting my whole family, and for teaching me to love others as myself.

Finally, I wish to dedicate this work to my whole family. I am very grateful to my parents, Tan Tai and Thi Anh, and grandparents for their love, support, sacrifices and never-ending prayers. I am thankful to my younger sisters, Xuan Trang and Ngoc Linh, for their love, and for looking after many things in my absence. Thanks also go to all my uncles and my aunts for their love and support. I wish to express my profound gratitude to my wife, Thanh Hoang, and my little son, Hoang Minh, for giving me their unwavering love, support, sacrifices and the time which I have stolen from them.

### Contents

Abstracti
Acknowledgementsiii
Contents v
List of Figures ix
List of Tables xvi
Chapter 1 Introduction 1
1.1 Problem statement
1.2 Object and scope
1.3 Contribution of the thesis
1.4 List of publications
1.4.1 Related journal articles
1.4.2 Related peer reviewed conference papers
1.4.3 Other publications
Chapter 2 literature Review
2.1 Introduction
2.2 Passive control systems
2.3 Active control systems
2.4 Semiactive control systems
2.5 Hybrid control systems
2.5 Summary
Chapter 3 MR Fluids and Devices

3.1 I	ntroduction	37
3.2 N	MR fluids	38
3.3 N	MR devices and applications	42
3.4 N	Modelling of MR dampers	48
3.4 (	Control of MR dampers	56
3.4 \$	Summary	68
Chapter 4 I	Genetic Algorithm and Its Application in Modelling of a Magr Rheological Damper	ieto- 70
4.1 I	ntroduction	70
4.2 0	Genetic algorithms	71
	4.2.1 Traditional GA pseudocode	71
	4.2.2 Strengths and weaknesses	72
	4.2.3 Applications of GAs in Modelling and Control	72
4.3 H	Proposed non-symmetric hysteresis Bouc-Wen model	73
	4.3.1 MR damper and Bouc-Wen model parameters	73
	4.3.2 Non-symmetric hysteresis Bouc-Wen model	79
4.4 I	dentification by Proposed Computationally-Efficient GA	81
	4.4.1 Chromosome structure	81
	4.4.2 Fitness function	82
	4.4.3 Selection	84
	4.4.4 Crossover and mutation	84
	4.4.5 Elitism	. 87
	4.4.6 Termination	. 87
4.5 F	Results	. 91
4.6 S	ummary	101

Chapter 5 Particle Swarm Optimisation and Polynomial Fitting Approach in		
Modelling of MR Dampers		
5.1 Introduction		
5.2 Particle Swarm Optimisation Technique		
5.3 Static Hysteresis Model of MR damper		
5.3.1 Parameter Identification by PSO		
5.3.2 Parameters against Supplied Current		
5.4 Polynomial fitting model of MR damper		
5.4.1 Mean value of the hysteresis		
5.4.2 Thickness of the hysteresis		
5.4.3 Proposed model		
5.4.4 Results and discussions		
5.5 Summary		
Chapter 6 Structural Control Approaches 127		
6.1 Introduction		
6.2 Structural System		
5.3.1 Damper Differential Configuration		
5.3.2 MR Damper-Embedded Structure Dynamics		
6.3 Lyapunov-based controller design		
6.4 LQR-based controller design		
6.5 Numerical Results and Discussions		
6.5.1 Evaluation Criteria		
6.5.2 Control responses		
6.5.2.1 Lyapunov-based control		
6.5.2.2 LOR-based direct control		

6.5.2.3 Discussions
6.6 Summary 153
Chapter 7 Seismic Structural Response Reduction Using MR Dampers 155
7.1 Introduction
7.2 Experimental Preparation156
7.2.1 One-Floor Steel Frame Building Model
7.2.2 Tools for Controller Development
7.3 Shake Table Tests
7.3.1 UTS shake table
7.3.2 Programming for tests
7.3.3 Results from tests using sinusoidal excitation 169
7.3.4 Results from test using benchmark earthquake excitations 173
7.4 Summary
Chapter 8 Conclusion and Future Work
8.1 Introduction
8.2 Summary of Thesis
8.2.1 Modelling of MR dampers
8.2.2 Control of MR dampers
8.3 Future Work 190
Bibliography

# **List of Figures**

1.1	A bank building in Beichuan after earthquake [159]2
1.2	Olive View Hospital after the earthquake in San Fernando, California, in
	1971 [5]
1.3	Rebuilt Olive View Hospital survived 1994 Northridge earthquake [5] 3
1.4	The USC University Hospital with base isolators [5]
2.1	Conventional and passive control
2.2	Tuned Mass Damper 16
2.3	Examples of structures equipped with tuned mass dampers
2.4	Tuned liquid damper and tuned liquid column damper [from 88] 17
2.5	X-Plate Metallic Damper (a), Triangular ADAS (b), and the former device
	installed in the structure (c) [from 6] 18
2.6	Examples of applications of viscous dampers to bridges [from 31]19
2.7	Pall Friction Damper
2.8	Base isolation system [94]
2.9	Section of a Laminated (a) and Lead Rubber Bearings (b) 20
2.10	Active control system
2.11	AMD control system [from 77]
2.12(a)	Kyobashi Seiwa Building [from 67]
2.12(b)	AMD-based control of Kyobashi Seiwa Building, Tokyo, Japan [from 67]23
2.13	Active mass damper using a rooftop heliport in the Applause Tower, Osaka, Japan
2.14	Semiactive control system
2.15	Interstate 35 Walnut Creek Bridge with variable-orifice dampers [58]

2.16	Semi-active TLCD system [from 91]27
2.17	Kajima Technical Research Institute Building equipped with variable-stiffness control devices [78]
2.18	Semi-active devices: (a) variable orifice dampers; (b) variable friction dampers; (c) adjustable tuned liquid dampers and (d) controllable fluid dampers [94]
2.19	Semi-active hydraulic dampers installed in the Kajima Shizuoka Building [40]
2.20	Nihon-Kagaku-Miraikan, Tokyo National Museum of Emerging Science and Innovation, installed with 30-t MR fluid dampers manufactured by Sawan Tekki Corporation [76]
2.21	Dongting Lake Bridge (a) and MR Dampers (b) in Hunan, China Dongting Lake Bridge in Hunan, China
2.22	Full-scale implementation of hybrid control device
2.23	Hybrid control system
2.24	Shinsuku Park Tower installed with V-shaped HMDs [94]
2.25	Smart base isolation system
3.1	MR fluid without (left) and with magnetic field (right)
3.2	Microscope images of MRF-132AD Lord Corporation before and after activation [113]
3.3	MR Fluid Behaviour (LORD Corporation 1997-2008)
3.4	A single chain behaviour under the vertically applied magnetic field with slowly increasing magnitude <i>B</i> [114]
3.5(a)	Yield stress vs. magnetic field strength of MRF-122-2ED (LORD Corporation)
3.5(b)	Magnetic properties of MRF-122-2ED (LORD Corporation)
3.6	Typical modes for MR fluid devices [8]

х

3.7	Small-scale SD-1000 MR Fluid Damper [94]
3.8	Large-scale 20t-MR Fluid Damper [94] 44
3.9	MR damper RD-1005-3
3.10	MR dampers installed in a bridge
3.11	Example of MR dampers installed in a building structure
3.12	MR damper embedded in a washing machine
3.13	MR damper used in lower leg prosthesis
3.14	Heavy duty seat suspension with MR damper
3.15	Characteristics of damper force vs. supply current: (a) non-linearity in force-displacement and (b) hysteresis in force-velocity
3.16	Bingham model of a fluid damper [122-123] 50
3.17	Comparison between the Bingham model and experimental results [75] 51
3.18	Extended Bingham model [110] 52
3.19	Comparison between the extended Bingham model and experimental results
	[75]
3.20	[75]
3.20 3.21	[75]53Bouc-Wen model of MR Damper54Comparison between the Bouc-Wen model and experimental results54
3.20 3.21 3.22	[75]53Bouc-Wen model of MR Damper54Comparison between the Bouc-Wen model and experimental results54Modified Bouc-Wen model of MR Damper55
<ul><li>3.20</li><li>3.21</li><li>3.22</li><li>3.23</li></ul>	[75]53Bouc-Wen model of MR Damper54Comparison between the Bouc-Wen model and experimental results54Modified Bouc-Wen model of MR Damper55Comparison between the modified Bouc-Wen model and experimental results [75]56
<ul> <li>3.20</li> <li>3.21</li> <li>3.22</li> <li>3.23</li> <li>3.24</li> </ul>	[75]53Bouc-Wen model of MR Damper54Comparison between the Bouc-Wen model and experimental results54Modified Bouc-Wen model of MR Damper55Comparison between the modified Bouc-Wen model and experimental results [75]56LQR and inverse Neural Network model of MR damper [107, 130]60
<ul> <li>3.20</li> <li>3.21</li> <li>3.22</li> <li>3.23</li> <li>3.24</li> <li>3.25</li> </ul>	[75]53Bouc-Wen model of MR Damper54Comparison between the Bouc-Wen model and experimental results54Modified Bouc-Wen model of MR Damper55Comparison between the modified Bouc-Wen model and experimental results [75]56LQR and inverse Neural Network model of MR damper [107, 130]60Block diagram of clipped-optimal control [21]61
<ul> <li>3.20</li> <li>3.21</li> <li>3.22</li> <li>3.23</li> <li>3.24</li> <li>3.25</li> <li>3.26</li> </ul>	[75]53Bouc-Wen model of MR Damper54Comparison between the Bouc-Wen model and experimental results54Modified Bouc-Wen model of MR Damper55Comparison between the modified Bouc-Wen model and experimental results [75]56LQR and inverse Neural Network model of MR damper [107, 130]60Block diagram of clipped-optimal control [21]61Clipped-optimal control [21]62
<ul> <li>3.20</li> <li>3.21</li> <li>3.22</li> <li>3.23</li> <li>3.24</li> <li>3.25</li> <li>3.26</li> <li>3.27</li> </ul>	[75]53Bouc-Wen model of MR Damper54Comparison between the Bouc-Wen model and experimental results54Modified Bouc-Wen model of MR Damper55Comparison between the modified Bouc-Wen model and experimental results [75]56LQR and inverse Neural Network model of MR damper [107, 130]60Block diagram of clipped-optimal control [21]61Clipped-optimal control [21]62Modified clipped-optimal control [101]63
<ul> <li>3.20</li> <li>3.21</li> <li>3.22</li> <li>3.23</li> <li>3.24</li> <li>3.25</li> <li>3.26</li> <li>3.27</li> <li>3.28</li> </ul>	[75]53Bouc-Wen model of MR Damper54Comparison between the Bouc-Wen model and experimental results54Modified Bouc-Wen model of MR Damper55Comparison between the modified Bouc-Wen model and experimental results [75]56LQR and inverse Neural Network model of MR damper [107, 130]60Block diagram of clipped-optimal control [21]61Clipped-optimal control [21]62Modified clipped-optimal control [101]63Another modified version of clipped-optimal control [116]63

4.2	MR damper displacement
4.3	MR damper force
4.4	MR damper force/displacement
4.5	MR damper force/velocity
4.6	Effect of parameters on hysteresis
4.7	Typical shifted hysteresis
4.8	MR damper parameter identification by GA 81
4.9	Termination based on the trace of minimum error
4.10	Hysteresis reconstructed from identified parameters: Bouc-Wen model; standard GA. Dotted line () represents experimental data and solid line (-) represents simulated reconstructed hysteresis
4.11	Hysteresis reconstructed from identified parameters: Bouc-Wen model; efficient GA. Dotted line () represents experimental data and solid line (-) represents simulated reconstructed hysteresis
4.12	Hysteresis reconstructed from identified parameters: Non-symmetric Bouc- Wen model; standard GA. Dotted line () represents experimental data and solid line (-) represents simulated reconstructed hysteresis
4.13	Hysteresis reconstructed from identified parameters: Non-symmetric Bouc- Wen model; efficient GA. Dotted line () represents experimental data and solid line (-) represents simulated reconstructed hysteresis
4.14	Analysis of identification results: Bouc-Wen model and standard GA (°); Bouc-Wen model and efficient GA (◊); non-symmetric Bouc-Wen model and standard GA (∇); non-symmetric Bouc-Wen model and standard GA (□).99
4.15	Reconstructed hysteresis from identified parameters. Dotted line () represents experimental data and solid line (-) represents simulated constructed hysteresis
5.1	Hysteresis parameters
5.2	Reconstructed static hysteretic model and experimental results

5.3	Reconstructed hysteresis from Bouc-Wen model 112
5.4	Parameter identification results (—) and polynomial fitted coefficients (· · ·): (a) parameter $c$ , (b) parameter $k$ , (c) parameter $\alpha$ , (d) parameter $\beta$ , (e) parameter $\delta$ , and (f) parameter $f_0$
5.5	Results of parameter identification. Experimental data ( $\cdot \cdot \cdot$ ), reconstructed hysteresis from polynomial fitted parameters (—): (a) frequency = 1 Hz, displacement = 8mm and (b) frequency = 2 Hz, displacement = 4 mm 117
5.6	Thickness curve
5.7	Thickness and mean 119
5.8	Comparison between this model and Bouc-Wen model and experimental results
5.9	RMS error vs. supplied current
5.10	Typical current versus parameters value, frequency =1Hz 122
5.11	Comparison of hysteresis from experimental (dotted) and simulated data (solid) - test 1
5.12	Comparison of hysteresis from experimental (dotted) and simulated data (solid) - test 2
6.1	System schematic diagram
6.2	Damper differential configuration
6.3	El-Centro responses: (a) earthquake record, (b) current, (c) damper force, (d) Lyapunov function, (e) 1st storey displacement, velocity & acceleration (dotted - no control, solid - under proposed Lyapunov-based control (Control 1))
6.4	<ul><li>Hachinohe responses: (a) earthquake record, (b) current, (c) damper force,</li><li>(d) Lyapunov function, (e) 1st storey displacement, velocity &amp; acceleration</li><li>(dotted - no control, solid - under Control 1)</li></ul>

xiii

6.5	Kobe responses: (a) earthquake record, (b) current, (c) damper force, (d) Lyapunov function, (e) 1st storey displacement, velocity & acceleration (dotted - no control, solid - under Control 1)
6.6	Northridge responses: (a) earthquake record, (b) current, (c) damper force, (d) Lyapunov function, (e) 1st storey displacement, velocity & acceleration (dotted - no control, solid - under Control 1)
6.7	El-Centro responses: (a) current, (b) damper force, (c) 1st storey displacement, velocity & acceleration (dotted - no control, solid - under proposed LQR- based control (Control 2))
6.8	Hachinohe responses: (a) current, (b) damper force, (c) 1st storey displacement, velocity & acceleration (dotted - no control, solid - under Control 2)
6.9	Kobe responses: (a) current, (b) damper force, (c) 1st storey displacement, velocity & acceleration (dotted - no control, solid - under Control 2) 149
6.10	Northridge responses: (a) current, (b) damper force, (c) 1st storey displacement, velocity & acceleration (dotted - no control, solid - under Control 2)
7.1	MR damper control set-up
7.2	Free vibration
7.3	Fourier spectrum
7.4	Block diagram of the DS1004 controller board 161
7.5	RTI and block diagram of a control system 161
7.6	ControlDest for acquiring data and observing interested signals 162
7.7	Damper disconnected
7.8	Passive control
7.9	Clipped-optimal control
7.10	Lyapunov-based control

7.11	Test signal
7.12	Experimental responses: Beam displacement for $i=0$ (dotted line) and $i=0.25$ A (solid line)
7.13	Experimental responses: (a) Beam displacement (dotted line- passive control (current 0A); solid line- Lyapunov-based control), (b) Damper current generated by Lyapunov-based control
7.14	Comparison of experimental responses: (a) Beam displacement, (b) Dampercurrent(dottedlines-clipped-optimalcontrol;solid lines-Lyapunov-based control)
7.15	Scaled Kobe earthquake
7.16	Beam displacement with no control (Kobe earthquake) 174
7.17	Beam displacement with proposed control (Koke earthquake) 175
7.18	Damper current proposed control (Koke earthquake) 175
7.19	Scaled El-Centro earthquake
7.20	Beam displacement with no control (El-Centro earthquake) 177
7.21	Beam displacement with proposed control (El-Centro earthquake) 177
7.22	Damper current with proposed control (El-Centro earthquake) 178
7.23	Scaled Hachinobe earthquake
7.24	Beam displacement with no control (Hachinobe earthquake) 179
7.25	Beam displacement with proposed control (Hachinobe earthquake)
7.26	Damper current with proposed control (Hachinobe earthquake)
7.27	Scaled Northridge earthquake
7.28	Beam displacement with no control (Northridge earthquake) 181
7.28	Beam displacement with proposed control (Northridge earthquake) 181
7.29	Damper current with proposed control (Northridge earthquake)

## **List of Tables**

2.1	List of Applications of TMDs, TLDs and AMDs [7]
3.1	Properties of three different types of LORD MR fluids (LORD Corporation)
3.2	Typical properties of ER and MR fluids [44] 42
3.3	Parameters of the 20-ton MR damper 43
4.1	Experimental setup for data gathering
4.2	Average error and standard deviation
4.3	Identification error below 95%
4.4	Expected terminating generation and likelihood terminating generation 97
5.1	Test conditions
5.2	Identified MR damper parameter vs. current at frequency = 1 Hz 125
5.3	Identified MR damper parameter vs. current at frequency = 2 Hz 125
6.1	Comparisons of the evaluation ratios between the passive control case of the damper current $i = 0$ and the proposed Lyapunov-based controller responses
6.2	Comparisons of the evaluation ratios between the passive control case of the damper current $i = 0$ and the proposed LQR-based controller responses 151
7.1	Parameters of the testing model with dampers disconnected (no control) 160
7.2	Properties of UTS shake table